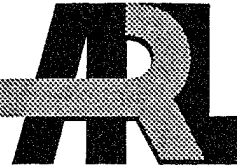


ARMY RESEARCH LABORATORY



A Method for Characterizing the Infrared Emissions From Kinetic Energy Penetrators

Thomas Kottke

ARL-MR-329

August 1996

19960819 034

APPROVED FOR PUBLIC RELEASE; DISTRIBUTION IS UNLIMITED.

NOTICES

Destroy this report when it is no longer needed. DO NOT return it to the originator.

Additional copies of this report may be obtained from the National Technical Information Service, U.S. Department of Commerce, 5285 Port Royal Road, Springfield, VA 22161.

The findings of this report are not to be construed as an official Department of the Army position, unless so designated by other authorized documents.

The use of trade names or manufacturers' names in this report does not constitute indorsement of any commercial product.

REPORT DOCUMENTATION PAGE			Form Approved OMB No. 0704-0188	
Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project(0704-0188), Washington, DC 20503.				
1. AGENCY USE ONLY (Leave blank)		2. REPORT DATE August 1996		3. REPORT TYPE AND DATES COVERED Final, Mar - Nov 95
4. TITLE AND SUBTITLE A Method for Characterizing the Infrared Emissions From Kinetic Energy Penetrators			5. FUNDING NUMBERS PR: 1L161102AH43	
6. AUTHOR(S) Thomas Kottke				
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) U.S. Army Research Laboratory ATTN: AMSRL-WT-WC Aberdeen Proving Ground, MD 21005-5066			8. PERFORMING ORGANIZATION REPORT NUMBER ARL-MR-329	
9. SPONSORING/MONITORING AGENCY NAMES(S) AND ADDRESS(ES)			10. SPONSORING/MONITORING AGENCY REPORT NUMBER	
11. SUPPLEMENTARY NOTES				
12a. DISTRIBUTION/AVAILABILITY STATEMENT Approved for public release; distribution is unlimited.			12b. DISTRIBUTION CODE	
13. ABSTRACT (Maximum 200 words) A method is presented for characterizing the infrared (IR) emissions from kinetic energy (KE) penetrators. This two-step computer simulation method first generates a faceted surface model of the penetrator of interest and then computes the associated IR signature. The IR emission from each facet is individually computed and then the emissions from the facets are summed. This approach allows both the spectral distribution and spatial distribution of the IR radiation emission to be determined. The methods for generating a facet model and computing the radiometric quantities are presented in detail. Verification testing of this software is also demonstrated. These computer programs have been written to run on IBM-compatible personal computer (PC) platforms. In order to encourage the migration and application of these routines by other investigators, highly documented code listings of these modular programs have been included in the appendices.				
14. SUBJECT TERMS infrared (IR) emission, IR radiation, modeling, kinetic energy penetrator			15. NUMBER OF PAGES 85	
			16. PRICE CODE	
17. SECURITY CLASSIFICATION OF REPORT UNCLASSIFIED	18. SECURITY CLASSIFICATION OF THIS PAGE UNCLASSIFIED	19. SECURITY CLASSIFICATION OF ABSTRACT UNCLASSIFIED	20. LIMITATION OF ABSTRACT UL	

INTENTIONALLY LEFT BLANK.

ACKNOWLEDGMENTS

The author would like to thank Mr. Charles R. Stumpfel of the Survivability Concepts Branch (SCB) for helpful discussions concerning radiometry theory and for carefully reviewing the technical details of this report along with Dr. Denis F. Strenzwilk (SCB). The author would also like to thank Ms. Mary Pfeiffer and Mrs. Tracey Mummert of LB&B Associates, Inc. for reviewing and polishing the final manuscript.

INTENTIONALLY LEFT BLANK.

TABLE OF CONTENTS

		<u>Page</u>
	ACKNOWLEDGMENTS	iii
	LIST OF FIGURES	vii
	LIST OF TABLES	vii
1.	INTRODUCTION	1
2.	PENETRATOR MODEL GENERATION	1
2.1	Penetrator Model Generation Overview	1
2.2	Conical Nose Cone Generation	2
2.3	Cylindrical Body Generation	4
2.4	Fin Generation	5
2.5	Aftbody Generation	7
2.6	Penetrator Surface Model Graphic Display	8
2.7	Penetrator Surface Model Temperature Assignment	10
3.	PENETRATOR IR EMISSION CALCULATION	11
3.1	Penetrator IR Emission Calculation Overview	11
3.2	Spectral Radiant Emittance	12
3.3	Spectral Radiance	14
3.4	Spectral Irradiance	15
3.5	Spectral Radiant Flux	17
3.6	Total Radiant Flux	18
3.7	IR Emission Analysis Software Verification	19
4.	SUMMARY	21
5.	REFERENCES	23
	APPENDIX A: PENETRATOR MODEL GENERATION SOFTWARE	25
	APPENDIX B: PENETRATOR IR EMISSION CALCULATION SOFTWARE ..	69
	DISTRIBUTION LIST	85

INTENTIONALLY LEFT BLANK.

LIST OF FIGURES

<u>Figure</u>	<u>Page</u>
1. Nose cone facet pattern and relevant program variables	3
2. Body facet pattern and relevant program variables	4
3. Fin facet pattern and relevant program variables	6
4. Aftbody facet pattern	8
5. Example of penetrator surface model graphic display	10

LIST OF TABLES

<u>Table</u>	<u>Page</u>
1. Comparison of Verification Radiant Flux Calculations	21

INTENTIONALLY LEFT BLANK.

1. INTRODUCTION

Temperatures of ballistic projectiles and kinetic energy (KE) penetrators in particular are elevated as they approach their impact points by in-bore heating during the launch phase and aerodynamic heating during the flight phase. The resulting emitted infrared (IR) radiation has been exploited as a means for tracking such penetrators (Thomson 1991). This method for projectile detection and tracking is particularly attractive because its inherently passive operation does not conflict with measures that may be employed to reduce armored vehicle signatures.

In order to utilize the IR radiation from penetrators for tracking purposes, it is necessary to characterize this radiation. Questions concerning the relative significance of various hot spots on the penetrator, the dependence of the IR signature on projectile orientation, the amount of signature variability introduced by projectile rotation, and requirements on detector and signal processing speed need to be addressed. This report presents a method for investigating these factors.

A two-step computer simulation process is presented that first generates a faceted surface model of the penetrator and then computes the associated IR signature by considering the IR emission from each individual facet. Both of these processes are presented in detail. A short primer is also included on radiometry. This should not be interpreted as an insult to the reader. Rather, this is presented as a common starting point in a field that is fraught with variability in both notation and definition.

In order to encourage the application of these routines by investigators in related studies, these programs have been written to run on IBM-compatible PC platforms. Highly documented code listings of these modular programs are included in the appendices.

2. PENETRATOR MODEL GENERATION

2.1 Penetrator Model Generation Overview. A first step in characterizing the IR energy emitted by a penetrator is to exercise an object generation program that creates a suitable computer model. Geometric details of the penetrator of interest are supplied as input to this program along with information about the temperature profile, thermal emissivities, orientation with

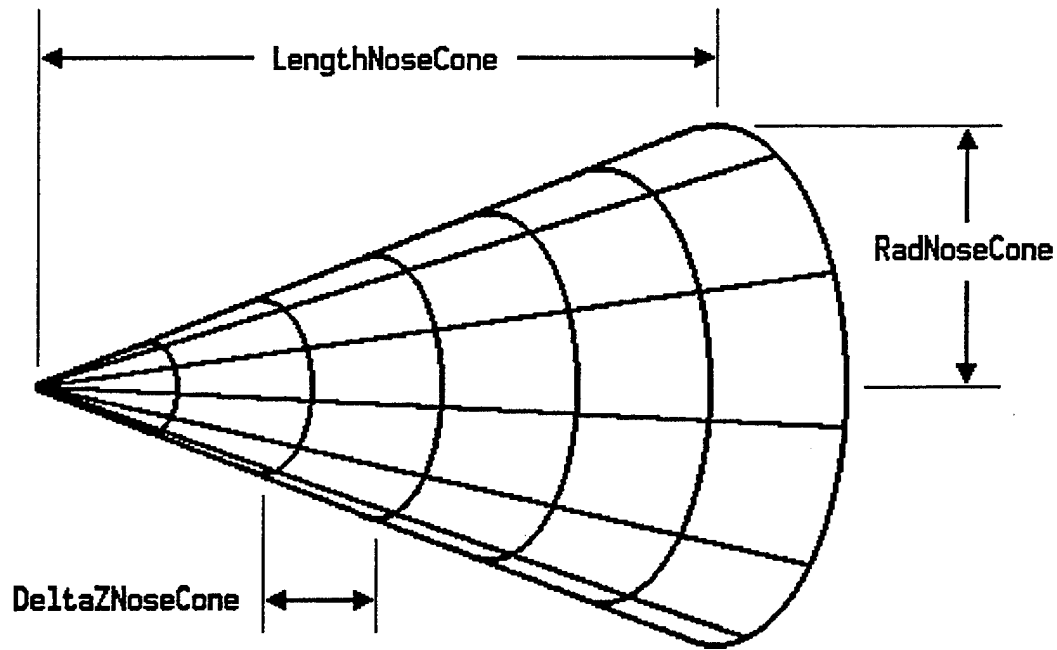
respect to the IR detector, and the manner in which the object is to be modeled. The program then generates a surface model of the penetrator that recreates the form as a collection of small planar surfaces, or facets. Each facet location and orientation is considered to determine whether or not it is visible at the location of the IR detector. A data file is constructed that records the location, orientation, area, temperature, and emissivity of all visible facets. This file can serve as the input to the IR spectrum calculation program that is described later.

The operation of the penetrator model generation software is now described in detail. A listing of this code is provided in Appendix A. Considerable effort has been expended to make the operation of this code readily understandable so that it may be easily modified and applied to a wide variety of applications. To achieve this goal, the program has been modularized through the use of subroutines, the listing has been extensively documented, and variable names have been utilized that describe their function or meaning. An unfortunate consequence of this explicit presentation is the considerable length of the resultant listing. The author hopes that the clarity of this code will offset any disadvantages resulting from its bulk.

Modeling of a penetrator-shaped object is simplified by the inherent simplicity and symmetry of the generic penetrator. In essence, most penetrators can be described as a conical forward section connected to a cylindrical body with equally spaced fins projecting radially at the rear. The object model generation software subdivides the penetrator into similar sections. Generation of the conical nose cone will now be described in detail. This will be followed by descriptions of how the cylindrical body, the fins, and the body areas between the fins are generated.

2.2 Conical Nose Cone Generation. Figure 1 illustrates the manner in which the conical nose cone section is modeled and the meaning of some of the relevant program variables. The overall dimensions of the conical section are defined by the length and base radius through the variables *LengthNoseCone* and *RadNoseCone*, respectively. Modeling resolution is determined by the variables *DeltaZNoseCone* and *NumNoseConeRadSeg%*. *DeltaZNoseCone* defines the thickness of each transverse nose cone "slice." *NumNoseConeRadSeg%* determines the number of radially oriented nose cone facets in each transverse nose cone slice.

Using these parameters, the subroutine *CalcNoseConePos* calculates the positions of each nose cone facet's corners, the area of each facet, and the components of each facet's outward



$$\text{number of radial nose cone facet positions} = \text{NumNoseConeRadSeg}\%$$

Figure 1. Nose cone facet pattern and relevant program variables.

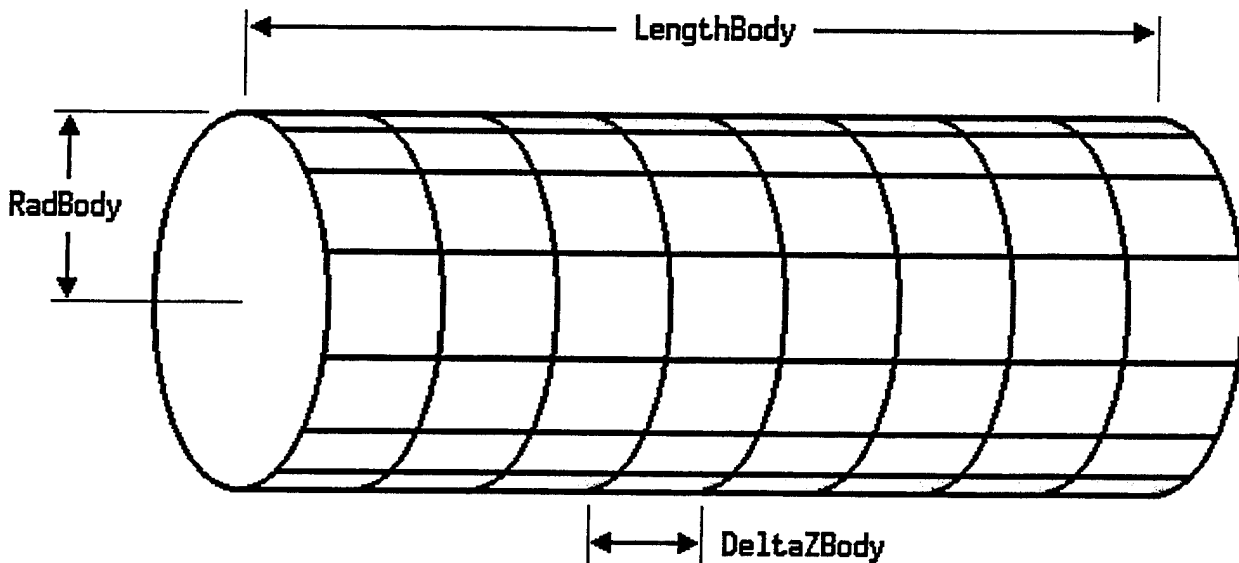
vector facing normal in body coordinates. Body coordinates are referenced to the penetrator with the z axis collocated with the penetrator's longitudinal axis and the x and y axes directed radially outward. The origin of the body coordinate system is taken as the tip of the nose cone with the positive z axis directed toward the rear of the penetrator. Calculation of the nose cone facet normal components is simplified by the fact that, due to the radial symmetry, the z component is the same for all of these facets.

The process of determining which nose cone facets are visible from the position of the IR detector is simplified by the assumption that the penetrator is always aimed toward the general direction of the IR detector. In this orientation, the conical nose cone will be closer to the detector than any other portion of the penetrator. Thus, no other portion of the penetrator can obscure any of the nose cone facets. Only the nose cone segments are capable of blocking other nose cone segments from the view of the IR detector. The simple symmetry of the conical nose cone allows the visibility of each facet to be determined by considering the orientation of the outward normal unit vector relative to the unit vector directed from the facet toward the IR detector. In particular, the dot product between these two unit vectors is computed. If this dot product is nonnegative,

then the facet's outward normal unit vector has a component directed toward the detector and the facet surface is visible to the detector. Facets for which this dot product is negative are facing away from the IR detector, and therefore the contribution of these facets to the overall IR spectrum can be disregarded.

2.3 Cylindrical Body Generation. The simple geometry of the cylindrical penetrator body allows the associated facet attributes to be readily calculated. This portion of the penetrator is assumed to extend from the base of the nose cone to the forwardmost fin position. Figure 2 displays the geometry of the cylindrical body and the significance of the relevant parameters. The length and radius of the penetrator body are defined by the parameters *LengthBody* and *RadBody*, respectively. Parameters *DeltaZBody* and *NumBodyRadSeg%* determine the size of each body facet and thus effectively control the resolution of the modeling for this portion of the penetrator.

The subroutine *CalcBodyPos* calculates the positions of the corners, the area, and the components of the outwardly facing normal unit vector for all the penetrator body facets in body coordinates. This task is simplified by the fact that the z component of the unit normal vectors is zero for all the body facets.



number of radial body facet positions = NumBodyRadSeg%

Figure 2. Body facet pattern and relevant program variables.

The assumption that the penetrator is aimed in the general direction of the IR detector also streamlines the process of determining which body facets are visible to the detector. Because the radius of any portion of the nose cone is always less than or equal to the body radius, the nose cone facets can never block any body facets that would otherwise be visible to the IR detector if the nose cone were removed. Therefore, the visibility of a body facet is also determined from the sign of the dot product between the facet's outward facing normal unit vector and the unit vector directed from the facet toward the detector.

2.4 Fin Generation. The fins are by far the most complex portion of the penetrator to be modeled. Figure 3 displays a generic fin and the parameters that define its shape and the manner in which a surface model is generated. The base length of the fin, where it attaches to the penetrator's body, is expressed by the variable *LengthBaseFin*. A forward portion of the fin is assumed to have a tapered profile. The extent of this tapered section is determined by the variable *LengthLeadEdgeFin*. *DeltaZFin* defines the size of the subdivisions along the z axis that the fin is partitioned into during the modeling process. The radial height of the fin is determined by the parameter *HeightFin*, and this length is subdivided into segments of dimension *DeltaRadFin*. Finally, the fin's thickness is quantified by the variable *ThickFin*. Facets along the edge of the fin that have a dimension defined by the variable *ThickFin* are referred to as edge facets. The remaining facets are referred to as side facets.

The corner positions, areas, and body coordinate components of the outward facing normal unit vectors are calculated by the subroutine *CalcFinPos* using the following simplifying observations.

- a) All the edge facets in the tapered portion of the fin have the same normal unit vector z component.
- b) All the edge facets in the tapered portion of the fin have the same area.
- c) All the edge facets in the nontapered portion of the fin have a normal unit vector z component of zero.
- d) All the edge facets in the nontapered portion of the fin have the same area.

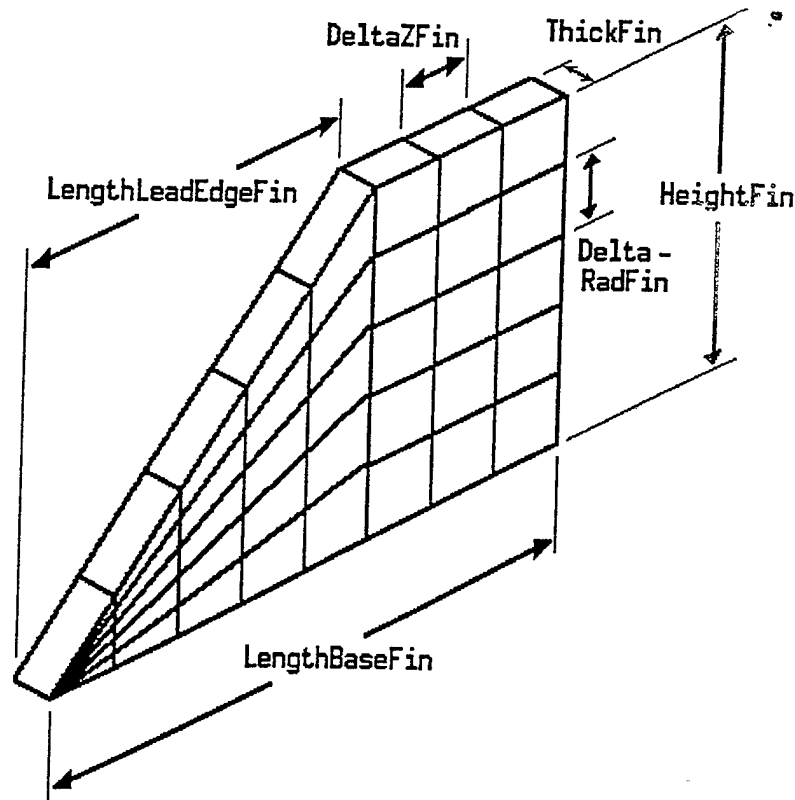


Figure 3. Fin facet pattern and relevant program variables.

- e) Because the penetrator is assumed to be aimed in the general direction of the IR detector, the trailing edge of the fin will never be visible, and therefore the edge facets on the trailing edge need not be considered.
- f) All the side facets have a normal unit vector z component of zero.
- g) All the side facets on one side of a given fin have the same normal unit vector x and y components.
- h) All the side facets in the nontapered portion of the fin have the same area.

The determination of which fin facets will be visible at the location of the IR detector is also somewhat involved. Recall that the visibility of the nose cone and body facets was determined by a simple vector dot product that, in essence, decided whether or not a facet surface pointed toward the IR detector. That is, the orientation of the detector relative to the penetrator precluded

the possibility that a facet in these portions of the penetrator could point toward the detector and still be blocked by another facet. This is not the case for the facets of the fin. Fin facets that point toward the detector may still not be visible to the detector because they are blocked by a facet in the nose cone, the body, the aftbody, or a facet on another fin. The aftbody portion of the penetrator has yet to be discussed. It is that portion of the penetrator body that is between the fins. Anyway, the subroutine *Eclipse* determines whether fin facets that point toward the detector are blocked by a facet in some other portion of the penetrator. Again, a number of observations are noted that streamline the associated calculations. Several of the following tests consider the fin's radial unit vector which is defined as the unit vector in the plane of the fin that is perpendicular to the z axis, or body, of the penetrator.

- a) A nose cone, body, or aftbody facet will never block a fin facet for which the dot product of the fin's radial unit vector with the unit vector directed from the facet toward the detector is positive. Fin facets in this category must still be checked for blockage by facets on other fins.
- b) A facet of a given fin with a surface that points toward the detector will never be blocked by another facet on that fin.
- c) The facets on a fin can only be blocked by the facets on another fin for which the dot product between the fin radial unit vector and the unit vector directed from the facet toward the viewer has a value that is closer to 1. In other words, a fin facet can only be blocked by the facets of fins that are in front of it, as viewed by the detector.
- d) An aftbody facet will never block a facet on a fin for which the dot product between the radial unit vector and the unit vector directed from the facet toward the viewer is nonnegative.

2.5 Aftbody Generation. The aftbody is that portion of the projectile body that is located between the fins. A representative aftbody area is illustrated in Figure 4. The overall longitudinal length and subdivision dimensions are the same as for the fins—namely *LengthBaseFin* and *DeltaZFin*, respectively. The tangential facet dimension is calculated from the circumference of the projectile body, the thickness of the fins, the total number of fins, and the number of radial facets between adjacent fins.

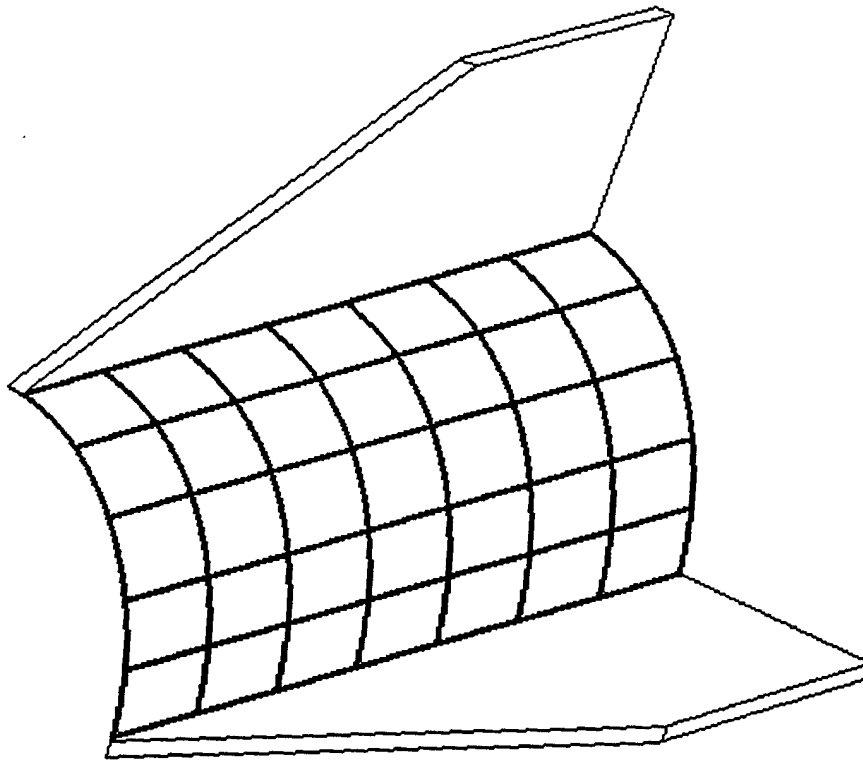


Figure 4. Aftbody facet pattern.

Aftbody facet corner positions, areas, and orientations, relative to the body coordinate system, are computed by the subroutine *CalcAftBodyPos*. These calculations are simplified by the fact that all the aftbody facets have the same area and a normal vector z component of zero. Each facet's orientation and the subroutine *Eclipse* are utilized to determine which aftbody facets are visible to the IR detector.

2.6 Penetrator Surface Model Graphic Display. After the facet corner positions and outward facing normal unit vector components have all been determined in the body coordinate system, an image of the penetrator is generated that illustrates the appearance of the penetrator from the vantage point of the IR detector. This process requires a transformation of all the facet corner positions from the body coordinate system of the penetrator to the space coordinate system of the detector. The origin of the space coordinate system is taken to be at the detector with the positive z axis extending horizontally to the right, the y axis extending vertically upward, and the x axis extending horizontally forward, relative to the detector's view of the penetrator. The transformation from body to space coordinates is accomplished by determining the Eulerian angles that relate the two coordinate systems and expressing the elements of the orthogonal transformation matrix as trigonometric functions of these angles (Goldstein 1950). Multiplication

of the body coordinate position vectors by the orthogonal transformation matrix yields the corresponding position vectors in the space coordinate system.

The perspective view of the penetrator is made more realistic by appropriate shading of the individual facets. Each facet position is displayed on the graphic image in a shade of gray that is determined from the facet's orientation relative to the viewpoint of the detector. In particular, the intensity of the shade of gray is proportional to the dot product between the facet's outward normal unit vector and the unit vector directed from the facet to the detector. This has the effect of imparting a dark coloration to facets that are seen on edge, while facets that are viewed face-on are displayed as a bright white. Thus, the illusion is created that light is glinting off appropriate portions of the penetrator from a light source that is collocated at the position of the detector. Although this effect is dramatic when displayed on a computer monitor, it does not show up well on printed hard copies. Therefore, a representative example of such an image is displayed in Figure 5 without the shading enhancement. This image was generated using the following penetrator input parameters.

nose cone length:	100 mm
nose cone longitudinal facet length:	10 mm
nose cone radius:	14 mm
number of nose cone radial facets:	24
body length:	420 mm
body longitudinal facet length:	20 mm
body radius:	14 mm
number of body radial facets:	24
number of fins:	6
fin thickness:	3 mm
fin total base length:	120 mm
fin leading edge base length:	80 mm
fin longitudinal facet length:	10 mm
fin height:	30 mm
fin transverse facet length:	5 mm
number of aftbody facets between adjacent fins:	4
Euler angles:	88.1°, 84.3°, 12°

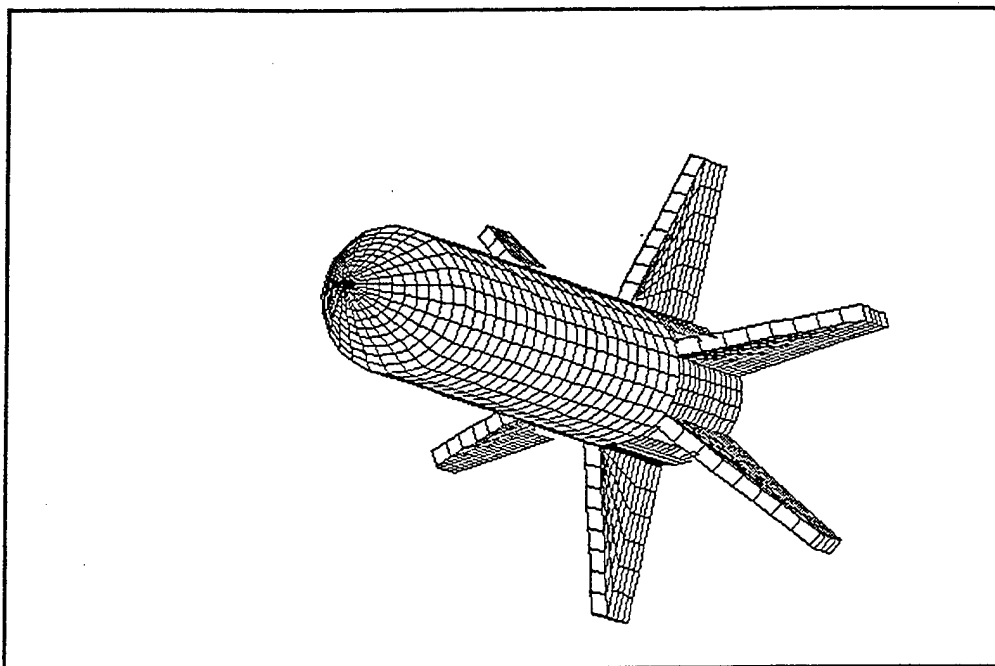


Figure 5. Example of penetrator surface model graphic display.

A graphical image of the penetrator is provided to the user as a quick "go/no go" check that the software is indeed modeling the intended scenario. Erroneous entry of penetrator dimension specifications are generally obvious from the resulting distorted image.

2.7 Penetrator Surface Model Temperature Assignment. The final computational task for the penetrator surface model generation software is the determination and allocation of a temperature to each facet. This is accomplished by interpolating between temperature values that are assigned to specific penetrator locations. In particular, the user must assign temperatures to the tip and base of the nose cone, the forward and rearmost body locations, the leading and trailing fin edges, the base fin position relative to the fin tip, and the forward and rearmost aftbody locations. Each facet's temperature is computed by determining its position relative to the appropriate defined temperature locations and interpolating a position-weighted intermediate temperature value. These calculations are handled by the subroutines *AssignNoseTemp*, *AssignBodyTemp*, *AssignFinSideTemp*, *AssignFinEdgeTemp*, and *AssignAftBodtTemp*. At the present time, these interpolations are a linear function of the facet's location between the defined boundary positions. In time, as computational or experimental determinations of actual penetrator flight temperatures become more quantitative, a more sophisticated interpolation process may be warranted. The modular nature of the temperature assignment subroutines will allow higher order interpolation techniques to be readily implemented.

A thermal emissivity is also assigned to each facet. This requires no computation. Rather, each facet within each region of the penetrator (nose cone, body, fin, or aftbody) is assumed to have the same direction-independent assigned thermal emissivity value. Directional emissivities are reserved for incorporation in future refinements of this process.

A data file is generated that contains the pertinent information about each penetrator surface facet. In particular, the recorded data include the region of the penetrator that the facet is located in, the facet corner positions in space coordinates, the value of the dot product between the facet's outward normal unit vector and the unit vector directed from the facet toward the detector, the area of the facet, the temperature of the facet, and the facet's thermal emissivity. Each data file includes an extensive leader that lists the geometric and thermal parameters that were used to generate the data set. This data file can be used as the input to the spectral calculation software that will be considered next.

3. PENETRATOR IR EMISSION CALCULATION

3.1 Penetrator IR Emission Calculation Overview. Recall that the goal of this modeling effort is to predict the amount and nature of the radiant energy that is generated by a heated penetrator and is collected by a suitable detector. To facilitate the required calculations, the penetrator has been modeled as a collection of surface facets. The approach is to separately consider the radiant energy that interacts with the detector from each facet and then sum these individual contributions to determine a total rate of radiant energy transfer. Effects arising from atmospheric absorption are not included due to the relatively short range over which IR sensors are expected to operate. The radiant energy transfer is characterized both spectrally and spatially. That is, the spectrum of the radiant energy that is emitted by various portions of the penetrator and incident upon the detector is determined. A detailed description of this process is now presented.

A newcomer to the field of radiometry is often bewildered by the abundance of terminology that, at first glance, appears to be describing the same thing. As an example, consider the fact that radiant energy, radiant energy density, radiant flux, radiant emittance, radiant photon emittance, radiant intensity, radiance, and irradiance are all terms that are commonly used to describe radiant energy transfer. In fact, this profusion of nomenclature arises from the need to consider a variety of scenarios involving radiation sources and detectors, both individually and

in combination, using a number of conventional normalization schemes. Luckily, a properly charted course will allow the reader, and even the author, to navigate this linguistic labyrinth.

The first task is to consider the spectral radiant emittance, which is the rate of radiant energy emission into a hemisphere per unit source area per unit wavelength interval at a particular wavelength. Already this is beginning to sound rather complicated. However, at this point the only considerations are the type and the rate at which radiant energy is coming off of a facet with no particular concern for where it is going. Clearly, the next step is to realize that the emitted radiation needs to go somewhere. This leads to a consideration of spectral radiance where not only the rate at which the radiant energy coming off a facet is addressed, but also the direction of that radiant energy. Up until this point, the facets have been treated as isolated sources. By finally introducing the detector into the scenario, the spectral irradiance can be calculated, which is a measure of the rate at which radiant energy from a facet is incident on the detector per unit detector area per unit wavelength interval at a particular wavelength. This is a general quantity because no assumptions have been made about the detector system. Additional radiometric quantities can be considered for specific detection apparatus.

If the collection area of the detector is known, the spectral radiant flux can be calculated. This is a measurement of the rate at which incident radiant energy enters the detector per unit wavelength interval at a particular wavelength. Of course, not all the radiant energy that enters the detector is necessarily recorded by the detector. If the spectral response of the detection system is known, then the total rate at which the detector records the incident radiant energy can be computed. This sounds a lot like the intermediate goal. So at this point a small victory will be declared, the same procedure will be followed for all the other facets, and all the individual facet contributions will be summed together. To keep things honest, the final result for a test case will be examined for validity to determine whether or not any celebrations were premature. So, with this radiometric roadmap in hand, the journey is begun by considering the spectral radiant emittance.

3.2 Spectral Radiant Emittance. All objects emit and absorb radiant energy. The quantity and character of this radiant energy depends on the temperature and nature of the object. A class of particularly convenient materials, known as black bodies, effectively absorb all incident radiant energy. Good absorbers of radiant energy also turn out to be good emitters. Thus, black

bodies are the best emitters of radiant energy. The spectral distribution of the radiant energy emitted by a black body is described by Planck's law,

$$W_{\lambda} = \frac{c_1}{\lambda^5} \frac{1}{e^{c_2/\lambda T} - 1} \quad (1)$$

where:

W_{λ} = spectral radiant emittance, $\text{W}\cdot\text{cm}^{-2}\cdot\mu\text{m}^{-1}$

λ = wavelength, μm

T = absolute temperature, K

C_1 = 3.742×10^4 , $\text{W}\cdot\text{cm}^{-2}\cdot\mu\text{m}^4$

C_2 = 1.439×10^4 , $\mu\text{m}\cdot\text{K}$.

In words, this expression calculates the radiant energy emitted by a black body of temperature T in a spectral band that is centered at wavelength λ per unit area per unit wavelength interval. Notice that this equation does not include any parameters that specify material properties of the emitting black body. This is in fact one of the conveniences associated with considering black body radiators. Black body radiation is totally dependent on the temperature of the black body and is totally independent of the particular material.

Unfortunately, most materials of unspecified configuration do not naturally exhibit black body characteristics. However, the spectral radiant emittance of objects that are not black bodies can be approximated by multiplying the expression of Equation 1 by an effective emissivity. An object's emissivity is a measure of its ability to emit radiant energy. Black bodies have an emissivity value of 1 while all other objects have an effective emissivity between 0 and 1. Emissivities can themselves be functions of both wavelength and temperature. Variations in spectral radiant emittance arising from an emissivity wavelength dependence are generally small compared to the strong wavelength dependence exhibited by Equation 1. The temperature dependence of the emissivity of representative metals has been shown to be weak over the temperature range 300–700 K (Snyder, Gier, and Dunkle 1955). It should also be noted that observed emissivity can depend on oxidation and mechanical surface treatments (Bramson 1968).

For all these reasons, and the fact that emissivity data in the literature is often sketchy at best, the use of a constant effective emissivity value is a common approximation.

3.3 Spectral Radiance. The next step is to consider where the radiant energy emitted by a facet is directed. At this point another common assumption is invoked that utilizes the angular distribution pattern of radiation emitted from perfectly diffuse sources. For such sources, known as Lambertian sources, the intensity of emitted radiation is proportional to the cosine of the angle between the surface normal and the emitted radiation direction of interest. When first encountered, this functional dependence for the radiation distribution pattern may appear somewhat arbitrary. However, recall that the effective projected area of a surface also depends on the cosine of the same angle. The spectral radiance of a perfectly diffuse source is therefore independent of viewing angle. A commonly cited example of a perfectly diffuse source is the sun. As predicted, the image of the sun appears to be uniformly bright in spite of the fact that the central portion is viewed face on while the edges are observed at a large angle from the solar surface normal.

Black bodies act as ideal diffuse sources. Real surfaces that are not black body radiators also tend to follow Lambert's cosine law quite closely at smaller viewing angles. However, at larger viewing angles, the amount of deviation from the ideal diffuse source radiation pattern is both material and surface topography dependent and can be significant (Hudson 1969).

As noted, one advantage in assuming a Lambertian source radiation pattern is the independence of the spectral radiance with respect to viewing angle. Another advantage is the fact that the spectral radiance from a surface radiating out into a hemisphere is related to the spectral radiant emittance by the simple relation

$$N_{\lambda} = W_{\lambda}/\pi \quad (2)$$

where:

W_{λ} = spectral radiant emittance, $W \cdot cm^{-2} \cdot \mu m^{-1}$

N_{λ} = spectral radiance, $W \cdot cm^{-2} \cdot sr^{-1} \cdot \mu m^{-1}$.

At this point it is worth digressing for a quick cautionary note. As stated, the Lambertian surface is assumed to radiate energy into a complete hemisphere of space. A hemisphere contains 2π steradians of solid angle. Therefore, a common impulse is to assume that the spectral radiant emittance and spectral radiance are related by a factor of 2π rather than the prescribed factor of π . As noted by Hudson (1969), "Of all the mistakes a newcomer to radiometry may make, confusion over this factor of 2 is an odds-on favourite." Avoiding this pitfall, we press on.

3.4 Spectral Irradiance. Having quantified the rate and the distribution of energy emitted by our radiant source, we are in a position to introduce the detector into the scenario and consider the rate at which radiant energy of a particular wavelength is incident on the detector per unit detector area per unit wavelength interval. The spectral irradiance at the detector can be related to the spectral radiance of the source facet using the relation (Brown 1992)

$$H_{\lambda} = A_{\text{source}} \cdot \Omega_{\text{det}} \cdot N_{\lambda} / A_{\text{det}} \quad (3)$$

where:

- H_{λ} = spectral irradiance, $\text{W} \cdot \text{cm}^{-2} \cdot \mu\text{m}^{-1}$
- A_{source} = effective source area, cm^2
- Ω_{det} = solid angle subtended by detector, sr
- N_{λ} = spectral radiance, $\text{W} \cdot \text{cm}^{-2} \cdot \text{sr}^{-1} \cdot \mu\text{m}^{-1}$
- A_{det} = effective detector area, cm^2 .

The first multiplicative factor on the right-hand side of Equation 3 is the effective area of the source. In this case, the source is the penetrator model facet under consideration. and the effective area is the area of the facet as "seen" by the detector. This effective area, or projected area, is obtained by multiplying the actual area of the facet by the cosine of the angle between the facet's outward normal vector and the normal vector directed from the facet to the detector. In equation form this can be expressed as

$$A_{\text{source}} = (\hat{n} \cdot \hat{r}) \cdot A_f \quad (4)$$

where:

- A_{source} = effective source area, cm^2
- \hat{n} = facet normal unit vector
- \hat{r} = unit vector directed from facet to detector
- A_f = facet area, cm^2 .

Conveniently, the areas of the facets and their outward normal components are included in the data file of information that is created by the previously discussed penetrator model generation software.

The second multiplicative factor on the right-hand side of Equation 3 is the solid angle subtended by the detector. A common definition for solid angle is

$$d\Omega = \frac{1}{r^2} dA \quad (5)$$

where:

- $d\Omega$ = incremental solid angle
- r = distance to the area
- dA = incremental area.

From this expression it is easy to see why spheres, with surface areas of $4\pi r^2$, are associated with a solid angle of 4π steradians. Some of the confusion surrounding solid angles may result from the fact that although they are expressed in units of steradians, they are in fact dimensionless quantities—as can be concluded from a dimensional check of Equation 5. Anyway, in order to determine the solid angle subtended by the detector, the distance from the source facet to the detector and the effective area of the detector must be known. For purposes

of calculation, the effective detector area is assumed to be 1 cm^2 . Therefore, the spectral irradiance can be expressed as

$$H_{\lambda} = (\hat{n} \cdot \hat{r}) \cdot A_f \cdot \frac{1}{r^2} \cdot N_{\lambda} \quad (6)$$

where:

- H_{λ} = spectral irradiance, $\text{W} \cdot \text{cm}^{-2} \cdot \mu\text{m}^{-1}$
- \hat{n} = facet normal unit vector
- \hat{r} = unit vector directed from facet to detector
- A_f = facet area, cm^2
- r = distance from facet to detector, cm
- N_{λ} = spectral radiance, $\text{W} \cdot \text{cm}^{-2} \cdot \mu\text{m}^{-1}$.

This formulation is general in the sense that it characterizes the nature of the radiation that is incident on the detector without making any assumptions about the detector itself.

3.5 Spectral Radiant Flux. Equation 6 is a generalized expression for the spectral irradiance at the site of a detector that is a distance r from a source facet. This is a measure of the rate at which energy is transferred to a unit area by radiation that is incident on that surface and that spans a specific interval of wavelengths. For a specific detector of known effective area, the spectral radiant flux can be determined. This is a measure of the rate at which radiant energy is conveyed to the detector position per unit wavelength interval at a particular wavelength. The spectral radiant flux can be determined from the spectral irradiance using the expression

$$P_{\lambda} = A_{\text{det}} \cdot H_{\lambda} \quad (7)$$

where:

$$\begin{aligned} P_{\lambda} &= \text{spectral radiant flux, W}\cdot\mu\text{m}^{-1} \\ A_{\text{det}} &= \text{detector area, cm}^2 \\ H_{\lambda} &= \text{spectral irradiance, W}\cdot\text{cm}^{-2}\cdot\mu\text{m}^{-1}. \end{aligned}$$

For application to specific systems where the detection spectral response is known, the total rate at which the detector accepts radiant energy, or total radiant flux, can be determined. A method for determining this quantity is now presented.

3.6 Total Radiant Flux. Having arrived at an expression for the rate at which radiant energy is incident on the detector at a particular wavelength, it is now possible to consider the total rate at which the detection system acquires radiant energy. This requires a knowledge of the spectral response of the detector system. In this case, the detector system response is assumed to include the effects of all focusing and filtering elements in addition to the conversion efficiency of the detector itself. The total radiant flux is computed by summing the spectral radiant flux, modulated by the detection system response, over a band of wavelengths that corresponds to the detector's active region.

Recall that the spectral radiant flux is defined as the rate of transfer of radiant energy per unit wavelength interval at a particular wavelength. Within a particular wavelength interval the spectral radiant flux is assumed to be constant. The strong wavelength dependence exhibited by Equation 1 suggests that this assumption is only valid over a narrow range of wavelengths. Therefore, in practice, the radiant emittance, radiance, irradiance, and radiant flux of broad wavelength regions are calculated by subdividing the region into many narrow subregions, calculating the spectral quantity of each subregion, and then summing the individual results. For a wavelength region extending from λ_1 to λ_2 that is divided into N subregions with central wavelength values of λ_i and wavelength spans of $(\Delta\lambda)_i$, the total radiant flux for a detector system with spectral response η_{λ_i} can be expressed as

$$P(\lambda_1 \rightarrow \lambda_2) = \sum_{i=1}^N \eta_{\lambda_i} \cdot P_{\lambda_i} \cdot (\Delta\lambda)_i. \quad (8)$$

At this point, one of the stated goals has been achieved. A method has been outlined for calculating the rate of radiant energy transfer, or radiant flux, between a single facet and a detector with a specified spectral response. The next step is to calculate the same quantity for various sections of the penetrator. Because the penetrator has been modeled as a collection of facets, this step is straightforward. The radiant flux is separately calculated for all the facets in a region of interest, and the individual results are summed together to yield the total radiant flux. The spectral analysis software that performs these functions is listed in Appendix B.

3.7 IR Emission Analysis Software Verification. The spectral analysis software is verified by comparing its results against the output from a commercially available software package that can calculate the IR emission spectrum for simple geometries. Integrated Sensors (Integrated Sensors, Inc. 1989) offers a disk-based IR spectrum calculator that computes the total flux and black body spectrum for sources with a specified temperature, range of emission wavelengths, emissivity, and field of view. Careful selection of input parameters for the penetrator generation and spectral analysis software presented in this report and Integrated Sensor's IR spectrum calculator can yield equivalent scenarios for which the outputs can be directly compared.

One such scenario is a circular source with a 10-mm radius located 10 m from a 1-cm² detector that accepts IR energy in the wavelength band from 2.0 μm to 5.5 μm . The following penetrator generation and spectrum analysis input parameters were used to create this case.

nose cone length	10 mm
nose cone longitudinal facet length	1 mm
nose cone radius	10 mm
number of nose cone radial facets	50
body length	20 mm
body longitudinal facet length	10 mm
body radius	10 mm
number of body radial facets	50
number of fins	1
fin thickness	1 mm
fin base length	10 mm
fin leading edge length	6 mm
fin longitudinal facet length	2 mm
fin height	4 mm

fin radial facet length	2 mm
number of aftbody facets between fins	1
Euler angles	90, 90, -90
nose cone tip temperature	573 K, 873 K, or 1,173 K
nose cone rear temperature	same as nose cone tip temperature
nose cone emissivity	0.1
body forward temperature	0 K
body rear temperature	0 K
body emissivity	0
fin leading edge temperature	1 K
fin trailing edge temperature	0 K
fin emissivity	0
aftbody forward temperature	0 K
aftbody rear temperature	0 K
aftbody emissivity	0
IR emission band	2.0 μm to 5.5 μm
calculation spectral window width	0.01 μm
penetrator range	10 m

These parameters yield a 10-mm radius penetrator that is aimed directly toward the detector. Thus, the nose cone appears circular to the detector. The extraneous body, fin, and aftbody penetrator components are effectively eliminated from the IR emission calculation by their assignment of very low temperatures and emissivities of 0. Three test cases are considered with nose cone temperatures of 573 K, 863 K, and 1,173 K.

The following inputs to Integrated Sensor's black body calculator yielded the equivalent scenario.

temperature	573 K, 873 K, or 1,173 K
wavelength band starting value	2.0 μm
wavelength band ending value	5.5 μm
emissivity	0.1
detector solid angle	1 E -6
source area	3.1416 cm^2

The results of the radiant flux calculations for the common scenario as determined using these two different programs are presented in Table 1.

Table 1. Comparison of Verification Radiant Flux Calculations

Temperature (K)	Results From Software Presented in This Report	Results From Integrated Sensor's Black Body Calculator
573	1.87E-8 W	1.87E-8 W
873	1.89E-7 W	1.89E-7 W
1,173	6.92E-7 W	6.91E-7 W

The close correlation between the results of these two IR emission calculation programs indicates that the results of the software presented in this report are numerically valid.

4. SUMMARY

A method is presented for characterizing the IR emissions from KE penetrators. Descriptions of this type are required for the application of IR tracker systems where questions concerning apparent source location, orientation effects, rotation effects, and detection speed need to be addressed. This two-step computer simulation method first generates a faceted surface model of the penetrator of interest and then computes the associated IR signature. The IR emission from each facet is individually computed. This approach allows both the spectral distribution and spatial distribution of the IR radiation emission to be determined. The methods for generating a facet model and computing the radiometric quantities are presented in detail. Verification testing of this software is also demonstrated.

These computer programs have been written to run on IBM-compatible PC platforms. In order to encourage the migration and application of these routines by other investigators, highly documented code listings of these modular programs have been included in the appendices. Future reports will highlight the results of IR characterization studies of specific scenarios.

INTENTIONALLY LEFT BLANK.

5. REFERENCES

- Bramson, M. A. Infrared Radiation, a Handbook for Applications. New York: Plenum Press, 1968.
- Brown, T. G. Radiometry and Detection. New York: University of Rochester, 1992.
- Goldstein, H. Classical Mechanics. Reading, MA: Addison-Wesley, 1950.
- Hudson, Jr., R. D. Infrared System Engineering. New York: Wiley-Interscience, 1969.
- Integrated Sensors, Inc. "Black Body Calculator, Version 1.3." Goleta, CA, 1989.
- Snyder, N. W., J. T. Gier, and R. V. Dunkle. "Total Normal Emissivity Measurements on Aircraft Materials Between 100 and 800° F." Transactions of the ASME, pp. 1011-1019, October 1955.
- Thomson, G. M. "Passive IR Tracking of Incoming Kinetic Energy Munitions." Proceedings of the 1991 BRL Technical Symposium: Emerging Technology for the Future Battlefield, Aberdeen Proving Ground, MD, November 1991.

INTENTIONALLY LEFT BLANK.

APPENDIX A:
PENETRATOR MODEL GENERATION SOFTWARE

INTENTIONALLY LEFT BLANK.

This software generates a facet model of a kinetic energy (KE) penetrator that can subsequently be used to calculate the spatial and spectral distributions of associated infrared (IR) emissions. MicroSoft QuickBasic 4.5 is used as the programming environment. If you have any questions about this code, please contact Tom Kottke at:

AMSRL-WT-WD
Survivability Concepts Branch
Weapons Concepts Division, Bldg. 120
Weapons Technology Directorate
U.S. Army Research Laboratory
Aberdeen Proving Ground, MD 21005-5066
(410) 278-2557

```

' the size of the arrays is allowed to
' change as required during execution

REM $DYNAMIC

' subroutines are declared

DECLARE SUB InputParameters ()
DECLARE SUB CalcNoseConePos ()
DECLARE SUB CalcBodyPos ()
DECLARE SUB CalcFinPos ()
DECLARE SUB CalcBoxExtremes ()
DECLARE SUB CalcEulerElem ()
DECLARE SUB TransCoordBS (XOld, YOld, ZOld, XSpace, YSpace, ZSpace)
DECLARE SUB TransCoordSB (XSpace, YSpace, ZSpace, XBody, YBody, ZBody)
DECLARE SUB CalcScreenSize ()
DECLARE SUB Init3DDisplay ()
DECLARE SUB DisplayBox ()
DECLARE SUB Plot3DPoint (X, Y, Z, C1)
DECLARE SUB Plot3DLine (X, Y, Z, C1)
DECLARE SUB Eclipse (XTest, YTest, ZTest, FinNumber%, FinUnitCOSValue, Type$, Ans%)
DECLARE SUB CalcFinEdgeMidPoint (FinNumber%, LeadEdgeLongSegNumber%, XMid, YMid,
                                ZMid)
DECLARE SUB CalcFinSideMidPoint (FinNumber%, LeadEdgeLongSegNumber%,
                                FinRadSegNumber%, SideNumber%, XMid, YMid, ZMid)
DECLARE SUB CalcAftBodyPos ()
DECLARE SUB CalcAftBodyMidPoint (ZSegment%, FinNumber%, AftBodyRadSegNumber%, XMid,
                                YMid, ZMid)
DECLARE SUB LoadDataFile (Type$, X(), Y(), Z(), NormalDotProduct, Area, Temp, Emis)
DECLARE SUB AssignNoseTemp (ZSegment%, NoseTemp)
DECLARE SUB AssignBodyTemp (ZSegment%, BodyTemp)
DECLARE SUB AssignFinSideTemp (LeadEdgeLongSegNumber%, FinRadSegNumber%, FinTemp)
DECLARE SUB AssignFinEdgeTemp (LeadEdgeLongSegNumber%, FinTemp)
DECLARE SUB AssignAftBodyTemp (ZSegment%, AftBodyTemp)

C1 = 1
DIM Euler(3)

CALL InputParameters

' projectile parameters are input
' array variables are dimensioned

DIM ZNoseConePos(NumNoseConeLongSeg%, 4)
DIM XNoseConePos(NumNoseConeLongSeg%, NumNoseConeRadSeg%, 4)
DIM YNoseConePos(NumNoseConeLongSeg%, NumNoseConeRadSeg%, 4)
DIM NoseConeArea(NumNoseConeLongSeg%)
DIM XNoseConeNormal(NumNoseConeRadSeg%)
DIM YNoseConeNormal(NumNoseConeRadSeg%)
DIM ZBodyPos(NumBodyLongSeg%, 4)

```

```

DIM XBodyPos(NumBodyRadSeg%, 4)
DIM YBodyPos(NumBodyRadSeg%, 4)
DIM XBodyNormal(NumBodyRadSeg%)
DIM YBodyNormal(NumBodyRadSeg%)
DIM E(3, 3)
DIM ZFinEdgePos(NumLeadEdgeLongSeg% + NumNonLeadEdgeLongSeg%, 4)
DIM YFinEdgePos(NumFins%, NumLeadEdgeLongSeg% + NumNonLeadEdgeLongSeg%, 4)
DIM XFinEdgePos(NumFins%, NumLeadEdgeLongSeg% + NumNonLeadEdgeLongSeg%, 4)
DIM ZFinPos(NumLeadEdgeLongSeg% + NumNonLeadEdgeLongSeg%, 4)
DIM YFinPos(NumFins%, NumLeadEdgeLongSeg% + NumNonLeadEdgeLongSeg%,
            NumFinRadSeg%, 2, 4)
DIM XFinPos(NumFins%, NumLeadEdgeLongSeg% + NumNonLeadEdgeLongSeg%,
            NumFinRadSeg%, 2, 4)
DIM XFinLeadEdgeNormal(NumFins%), XFinNonLeadEdgeNormal(NumFins%)
DIM YFinLeadEdgeNormal(NumFins%), YFinNonLeadEdgeNormal(NumFins%)
DIM XFinSideNormal(NumFins%, 2), YFinSideNormal(NumFins%, 2)
DIM ZAftBodyPos(NumLeadEdgeLongSeg% + NumNonLeadEdgeLongSeg%, 4)
DIM XAftBodyPos(NumFins%, NumAftBodyRadSegPerFin%, 4)
DIM YAftBodyPos(NumFins%, NumAftBodyRadSegPerFin%, 4)
DIM XAftBodyNormal(NumFins%, NumAftBodyRadSegPerFin%)
DIM YAftBodyNormal(NumFins%, NumAftBodyRadSegPerFin%)
DIM X(4), Y(4), Z(4), FinLeadSideArea(NumLeadEdgeLongSeg%)

ScreenWidth = 638
ScreenHeight = 398
AspectRatio = .97

CALL CalcNoseConePos
'nose cone facet coordinates, areas, and
'orientations are calculated

CALL CalcBodyPos
'body facet coordinates, areas, and
'orientations are calculated

CALL CalcFinPos
'fin facet coordinates, areas, and
'orientations are calculated

CALL CalcAftBodyPos
'afterbody facet coordinates, areas, and
'orientations are calculated

CALL CalcBoxExtremes
'determining the extreme positions

CALL CalcEulerElem
'the components of the normal vector
'pointing from the projectile's body
'coordinate origin to the viewer are
'calculated in the body coordinate
'system. note that the viewer's (or the
'computer monitor's) coordinate system
'has the positive x axis pointing into
'the screen, the positive y axis pointing
'up, and the positive z axis pointing
'toward the right.

CALL TransCoordSB(-1, 0, 0, XViewNormal, YViewNormal, ZViewNormal)
'an appropriate scale for the graphic
'display screen is determined

CALL CalcScreenSize
'the graphic display is initialized, the
'graphic display parameters are stored in
'the data file, and the display colors
'are defined

CALL Init3DDisplay

```

```
*****
THIS NEXT SECTION OF CODE PLOTS OUT ALL THE PROJECTILE FACETS USING THE
SUBTLE CONSTRUCTION LINE COLOR. LATER, THE VISIBLE FACETS WILL BE REDRAWN
USING A COLOR THAT REPRESENTS THEIR ORIENTATION RELATIVE TO THE VIEWER.
*****
```

```

                                'all the nose cone facets are plotted
                                'each transverse nose cone slice is
                                'considered
FOR ZSegment% = 0 TO NumNoseConeLongSeg% - 1
                                'each radial facet within the transverse
                                'slice is considered
FOR CordSegment% = 0 TO NumNoseConeRadSeg% - 1
                                'the first corner of each facet is plotted
                                'as a point
CALL TransCoordBS(XNoseConePos(ZSegment%, CordSegment%, 4),
                                YNoseConePos(ZSegment%, CordSegment%, 4),
                                ZNoseConePos(ZSegment%, 4), XSpace, YSpace, ZSpace)
CALL Plot3DPoint(XSpace, YSpace, ZSpace, 2)
                                'lines are drawn connecting all the
                                'corners
FOR Corner% = 1 TO 4
CALL TransCoordBS(XNoseConePos(ZSegment%, CordSegment%, Corner%),
                                YNoseConePos(ZSegment%, CordSegment%, Corner%),
                                ZNoseConePos(ZSegment%, Corner%), XSpace, YSpace,
                                ZSpace)
CALL Plot3DLine(XSpace, YSpace, ZSpace, 2)
NEXT Corner%
NEXT CordSegment%
NEXT ZSegment%

                                'all the body facets are plotted
                                'each transverse body slice is considered
FOR ZSegment% = 0 TO NumBodyLongSeg% - 1
                                'each radial facet within the transverse
                                'slice is considered
FOR CordSegment% = 0 TO NumBodyRadSeg% - 1
                                'the first corner of each facet is plotted
                                'as a point
CALL TransCoordBS(XBodyPos(CordSegment%, 4), YBodyPos(CordSegment%, 4),
                                ZBodyPos(ZSegment%, 4), XSpace,
                                YSpace, ZSpace)
CALL Plot3DPoint(XSpace, YSpace, ZSpace, 2)
                                'lines are drawn connecting all the
                                'corners
FOR Corner% = 1 TO 4
CALL TransCoordBS(XBodyPos(CordSegment%, Corner%),
                                YBodyPos(CordSegment%, Corner%),
                                ZBodyPos(ZSegment%, Corner%), XSpace,
                                YSpace, ZSpace)
CALL Plot3DLine(XSpace, YSpace, ZSpace, 2)
NEXT Corner%
NEXT CordSegment%
NEXT ZSegment%

                                'all the fin facets are plotted
                                'each fin is considered in turn
FOR FinNumber% = 0 TO NumFins% - 1
                                'each transverse fin slice is considered
FOR LeadEdgeLongSegNumber% = 0 TO NumLeadEdgeLongSeg% +
                                NumNonLeadEdgeLongSeg% - 1
                                'the side facets in each transverse
```

```

                                'slice are considered
FOR FinRadSegNumber% = 0 TO NumFinRadSeg% - 1
                                'both of the fin sides are considered
    FOR SideNumber% = 1 TO 2
                                'the first facet corner is plotted as
                                'a point
        CALL TransCoordBS(XFinPos(FinNumber%, LeadEdgeLongSegNumber%,
                                FinRadSegNumber%, SideNumber%, 4),
                                YFinPos(FinNumber%, LeadEdgeLongSegNumber%,
                                FinRadSegNumber%, SideNumber%, 4),
                                ZFinPos(LeadEdgeLongSegNumber%, 4), XSpace, YSpace,
                                ZSpace)
        CALL Plot3DPoint(XSpace, YSpace, ZSpace, 2)
                                'lines are drawn connecting all the
                                'corners
        FOR Corner% = 1 TO 4
            CALL TransCoordBS(XFinPos(FinNumber%, LeadEdgeLongSegNumber%,
                                FinRadSegNumber%, SideNumber%, Corner%),
                                YFinPos(FinNumber%, LeadEdgeLongSegNumber%,
                                FinRadSegNumber%, SideNumber%, Corner%),
                                ZFinPos(LeadEdgeLongSegNumber%,
                                Corner%), XSpace, YSpace, ZSpace)
            CALL Plot3DLine(XSpace, YSpace, ZSpace, 2)
        NEXT Corner%

    NEXT SideNumber%
NEXT FinRadSegNumber%

                                'the leading edge facet is considered
                                'the first facet corner is plotted as
                                'a point
CALL TransCoordBS(XFinEdgePos(FinNumber%, LeadEdgeLongSegNumber%, 4),
                                YFinEdgePos(FinNumber%, LeadEdgeLongSegNumber%, 4),
                                ZFinEdgePos(LeadEdgeLongSegNumber%, 4), XSpace,
                                YSpace, ZSpace)
CALL Plot3DPoint(XSpace, YSpace, ZSpace, 2)
                                'lines are drawn connecting all the
                                'corners
FOR Corner% = 1 TO 4
    CALL TransCoordBS(XFinEdgePos(FinNumber%, LeadEdgeLongSegNumber%,
                                Corner%), YFinEdgePos(FinNumber%,
                                LeadEdgeLongSegNumber%, Corner%),
                                ZFinEdgePos(LeadEdgeLongSegNumber%, Corner%), XSpace,
                                YSpace, ZSpace)
    CALL Plot3DLine(XSpace, YSpace, ZSpace, 2)
NEXT Corner%

NEXT LeadEdgeLongSegNumber%
NEXT FinNumber%

                                'all the aftbody facets are plotted
                                'each transverse aftbody slice is
                                'considered
FOR ZSegment% = 0 TO NumLeadEdgeLongSeg% + NumNonLeadEdgeLongSeg% - 1
                                'the afterbody region between each pair
                                'of adjacent fins is considered
    FOR FinNumber% = 0 TO NumFins% - 1
                                'each afterbody radial facet is considered
        FOR AftBodyRadSegNumber% = 0 TO NumAftBodyRadSegPerFin% - 1
                                'the first facet corner is plotted as
                                'a point
            CALL TransCoordBS(XAftBodyPos(FinNumber%, AftBodyRadSegNumber%, 4),
                                YAftBodyPos(FinNumber%, AftBodyRadSegNumber%, 4),
                                ZAftBodyPos(ZSegment%, 4), XSpace, YSpace, ZSpace)
            CALL Plot3DPoint(XSpace, YSpace, ZSpace, 2)
                                'lines are drawn connecting all the

```



```

'corners
FOR Corner% = 1 TO 4
  CALL TransCoordBS(XAftBodyPos(FinNumber%, AftBodyRadSegNumber%,
    Corner%), YAftBodyPos(FinNumber%,
    AftBodyRadSegNumber%, Corner%),
    ZAftBodyPos(ZSegment%, Corner%),
    XSpace, YSpace, ZSpace)
  CALL Plot3DLine(XSpace, YSpace, ZSpace, 2)
NEXT Corner%

NEXT AftBodyRadSegNumber%
NEXT FinNumber%
NEXT ZSegment%

```

'EACH PROJECTILE FACET IS RECONSIDERED TO DETERMINE WHETHER IT IS IN A
 'POSITION THAT IS VISIBLE TO THE VIEWER. THOSE FACETS THAT ARE VISIBLE ARE
 'REDRAWN USING A COLOR THAT REPRESENTS THE FACETS ORIENTATION WITH RESPECT
 'TO THE VIEWER. FACETS WITH A NORMAL VECTOR THAT POINTS DIRECTLY TOWARD THE
 'VIEWER ARE REPLOTTED USING WHITE LINES. FACETS WITH A NORMAL VECTOR THAT IS
 'PERPENDICULAR TO THE VIEWERS DIRECTION ARE REPLOTTED USING BLACK LINES.
 'FACETS WITH NORMAL VECTORS THAT FALL BETWEEN THESE TWO EXTREMES ARE
 'REPLOTTED USING AN APPROPRIATE SHADE OF GRAY. THIS COLORING SCHEME YIELDS AN
 'IMAGE OF THE PROJECTILE THAT MIMICS THE CASE WHERE THE ILLUMINATING LIGHT
 'SOURCE IS BETWEEN THE VIEWER'S EYES.

```

'all the nose cone facets are reconsidered

'each transverse nose cone slice is
'considered
FOR ZSegment% = 0 TO NumNoseConeLongSeg% - 1
  'each radial facet within the transverse
  'slice is considered
  FOR CordSegment% = 0 TO NumNoseConeRadSeg% - 1
    'the visibility of a facet to the viewer
    'is determined by considering the dot
    'product between the facet's outwardly
    'pointed normal vector and the normal
    'vector pointing towards the viewer. if
    'this dot product is positive, then the
    'facet is visible. it is assumed that no
    'other portion of the projectile will
    'ever block a nose cone facet.
    NormalDotProduct = XNoseConeNormal(CordSegment%) * XViewNormal +
      YNoseConeNormal(CordSegment%) * YViewNormal +
      ZNoseConeNormal * ZViewNormal
    IF (NormalDotProduct > 0) THEN
      'a corner of each visible facet is
      'plotted as a point
      CALL TransCoordBS(XNoseConePos(ZSegment%, CordSegment%, 4),
        YNoseConePos(ZSegment%, CordSegment%, 4),
        ZNoseConePos(ZSegment%, 4), XSpace, YSpace, ZSpace)
      CALL Plot3DPoint(XSpace, YSpace, ZSpace, NormalDotProduct * 12 + 3)
      'lines are drawn connecting the facer
      'corners

      FOR Corner% = 1 TO 4
        CALL TransCoordBS(XNoseConePos(ZSegment%, CordSegment%, Corner%),
          YNoseConePos(ZSegment%, CordSegment%, Corner%),
          ZNoseConePos(ZSegment%, Corner%), XSpace, YSpace,
          ZSpace)
        CALL Plot3DLine(XSpace, YSpace, ZSpace, NormalDotProduct * 12 + 3)
        'facet corner positions are saved for
        'later transfer to the data storage file

        X(Corner%) = XSpace
        Y(Corner%) = YSpace
      
```

```

    Z(Corner%) = ZSpace
    NEXT Corner%

    'the temperature of the facet is
    'determined by interpolation
    CALL AssignNoseTemp(ZSegment%, NoseTemp)
    'data is transferred to the storage file
    CALL LoadDataFile("Nose", X(), Y(), Z(), NormalDotProduct,
        NoseConeArea(ZSegment%), NoseTemp, NoseEmis)
    END IF
    NEXT CordSegment%
NEXT ZSegment%

    'all the body facets are reconsidered
    'each trasverse body slice is considered
FOR ZSegment% = 0 TO NumBodyLongSeg% - 1
    'each radial facet within the transverse
    'slice is considered
    FOR CordSegment% = 0 TO NumBodyRadSeg% - 1
        'the visibility of a facet to the viewer
        'is determined by considering the dot
        'product between the facets outwardly
        'pointed normal vector and the unit
        'vector pointing towards the viewer. if
        'this dot product is positive, then the
        'facet is visible. it is assumed that no
        'other portion of the projectile will
        'ever block a body facet.
        NormalDotProduct = XBodyNormal(CordSegment%) * XViewNormal +
            YBodyNormal(CordSegment%) * YViewNormal +
            ZBodyNormal * ZViewNormal
        IF (NormalDotProduct > 0) THEN
            'the first corner of each visible facet
            'is plotted as a point
            CALL TransCoordBS(XBodyPos(CordSegment%, 4), YBodyPos(CordSegment%, 4),
                ZBodyPos(ZSegment%, 4), XSpace, YSpace, ZSpace)
            CALL Plot3DPoint(XSpace, YSpace, ZSpace, NormalDotProduct * 12 + 3)
            'lines are drawn connecting all the
            'facet corners
            FOR Corner% = 1 TO 4
                CALL TransCoordBS(XBodyPos(CordSegment%, Corner%),
                    YBodyPos(CordSegment%, Corner%), ZBodyPos(ZSegment%,
                        Corner%), XSpace, YSpace, ZSpace)
                CALL Plot3DLine(XSpace, YSpace, ZSpace, NormalDotProduct * 12 + 3)
                'facet corner positions are saved for
                'later transfer to the storage data file

                X(Corner%) = XSpace
                Y(Corner%) = YSpace
                Z(Corner%) = ZSpace
            NEXT Corner%

            'the temperature of the facet is
            'determined by interpolation
            CALL AssignBodyTemp(ZSegment%, BodyTemp)
            'data is transferred to the storage file
            CALL LoadDataFile("Body", X(), Y(), Z(), NormalDotProduct, BodyArea, BodyTemp,
                BodyEmis)
        END IF
    NEXT CordSegment%
NEXT ZSegment%

    'all the fin facets are reconsidered
    'each fin is considered in turn
FOR FinNumber% = 0 TO NumFins% - 1
    'the x and y components in the body
    'coordinate system are calculated for
    'a unit vector lying in the plane of the
    'fin that is normal to the longitudinal

```

```

'axis
FinUnitRadXVector = -COS(2 * 3.14159 * FinNumber% / NumFins%)
FinUnitRadYVector = SIN(2 * 3.14159 * FinNumber% / NumFins%)
'each transverse fin slice is considered
'unit vector pointing towards the viewer.
'the resulting cosine value is a measure
'of the degree to which the fin points
'toward the viewer
FinUnitCOSValue = FinUnitRadXVector * XViewNormal + FinUnitRadYVector *
YViewNormal
'each transverse fin slice is considered
FOR LeadEdgeLongSegNumber% = 0 TO NumLeadEdgeLongSeg% +
NumNonLeadEdgeLongSeg% - 1
'the side facets in each transverse
'slice are considered
FOR FinRadSegNumber% = 0 TO NumFinRadSeg% - 1
'both of the fin sides are considered
FOR SideNumber% = 1 TO 2
'the visibility of a facet to the viewer
'is determined by first considering the
'dot product between the facet's outward
'pointed normal vector and the normal
'vector pointed towards the viewer. if
'this dot product is positive then the
'facet may be visible to the viewer.
NormalDotProduct = XFinSideNormal(FinNumber%, SideNumber%) * XViewNormal +
YFinSideNormal(FinNumber%, SideNumber%) * YViewNormal +
ZFinSideNormal * ZViewNormal
IF (NormalDotProduct > 0) THEN
'the areal midpoint position of the facet
'is calculated in the body coordinate
'system
CALL CalcFinSideMidPoint(FinNumber%, LeadEdgeLongSegNumber%,
FinRadSegNumber%, SideNumber%, XMid, YMid, ZMid)
'this midpoint position is then
'transformed to the space coordinate
'system
CALL TransCoordBS(XMid, YMid, ZMid, XSpace, YSpace, ZSpace)
'the graphic display plot color at this
'midpoint pixel position is saved
OldColor = POINT(ZSpace * Scale, YSpace * Scale)
'the midpoint pixel position is replotted
'in white to denote the facet under
'consideration
CALL Plot3DPoint(XSpace, YSpace, ZSpace, 15)
'all other projectile facets are
'considered to determine whether any of
'them will block the viewer's view of
'this facet
CALL Eclipse(XSpace, YSpace, ZSpace, FinNumber%, FinUnitCOSValue, "Fin",
Ans%)
'if the facet is not blocked by any other
'facet then the subroutine returns with
'the variable Ans% equal to 1
IF (Ans% = 1) THEN
'the midpoint position pixel is replotted
'in its original graphic display color
CALL Plot3DPoint(XSpace, YSpace, ZSpace, OldColor)
'a corner of the facet is plotted as a
'point
CALL TransCoordBS(XFinPos(FinNumber%, LeadEdgeLongSegNumber%,
FinRadSegNumber%, SideNumber%, 4),
YFinPos(FinNumber%, LeadEdgeLongSegNumber%,
FinRadSegNumber%, SideNumber%, 4),
ZFinPos(LeadEdgeLongSegNumber%, 4), XSpace, YSpace,
ZSpace)

```

```

CALL Plot3DPoint(XSpace, YSpace, ZSpace, NormalDotProduct * 12 + 3)
'lines are drawn between the facet corners
'using a display color that indicates the
'facets orientation with respect to the
'viewer

FOR Corner% = 1 TO 4
  CALL TransCoordBS(XFinPos(FinNumber%, LeadEdgeLongSegNumber%,
    FinRadSegNumber%, SideNumber%, Corner%),
    YFinPos(FinNumber%, LeadEdgeLongSegNumber%,
    FinRadSegNumber%, SideNumber%, Corner%), ZFinPos(
    LeadEdgeLongSegNumber%, Corner%), XSpace, YSpace,
    ZSpace)

  CALL Plot3DLine(XSpace, YSpace, ZSpace, NormalDotProduct * 12 + 3)
  'the facet corner positions are saved for
  'later transfer to the data storage file

  X(Corner%) = XSpace
  Y(Corner%) = YSpace
  Z(Corner%) = ZSpace
NEXT Corner%

'the temperature of the facet is
'determined by interpolation and the
'data is transferred to the storage file
IF (LeadEdgeLongSegNumber% < NumLeadEdgeLongSeg%) THEN
  CALL AssignFinSideTemp(LeadEdgeLongSegNumber%, FinRadSegNumber%,
    FinTemp)
  CALL LoadDataFile("Fin ", X(), Y(), Z(), NormalDotProduct,
    FinLeadSideArea(LeadEdgeLongSegNumber%), FinTemp,
    FinEmis)
ELSE
  CALL AssignFinSideTemp(LeadEdgeLongSegNumber%, FinRadSegNumber%,
    FinTemp)
  CALL LoadDataFile("Fin ", X(), Y(), Z(), NormalDotProduct,
    FinNonLeadSideArea, FinTemp, FinEmis)
END IF

'if the view of the facet is blocked by
'another facet the midpoint position
'pixel is simple returned to its
'original color
ELSE
  CALL Plot3DPoint(XSpace, YSpace, ZSpace, OldColor)
END IF
END IF
NEXT SideNumber%
NEXT FinRadSegNumber%

'the fin edge for this longitudinal fin
'slice is considered

'the dot product of the edge facets
'outward normal vector with the unit
'vector towards the viewer is calculated
IF (LeadEdgeLongSegNumber% < NumLeadEdgeLongSeg%) THEN
  NormalDotProduct = XFinLeadEdgeNormal(FinNumber%) * XViewNormal +
    YFinLeadEdgeNormal(FinNumber%) * YViewNormal +
    ZFinLeadEdgeNormal * ZViewNormal
ELSE
  NormalDotProduct = XFinNonLeadEdgeNormal(FinNumber%) * XViewNormal +
    YFinNonLeadEdgeNormal(FinNumber%) * YViewNormal
END IF

'this edge facet can only be visible if
'the dot product is positive
IF (NormalDotProduct > 0) THEN

'the midpoint of the edge facet is
'calculated in body coordinates
CALL CalcFinEdgeMidPoint(FinNumber%, LeadEdgeLongSegNumber%, XMid, YMid,
  ZMid)

```

```

                                'this midpoint position is transformed to
                                'space coordinates
CALL TransCoordBS(XMid, YMid, ZMid, XSpace, YSpace, ZSpace)
                                'the original color of this midpoint
                                'pixel position is saved
OldColor = POINT(ZSpace * Scale, YSpace * Scale)
                                'the midpoint position pixel is replotted
                                'in white to denote which facet is under
                                'consideration
CALL Plot3DPoint(XSpace, YSpace, ZSpace, 15)
                                'all other projectile facets are
                                'considered to determine whether any of
                                'them will block the viewer's view of
                                'this facet
CALL Eclipse(XSpace, YSpace, ZSpace, FinNumber%, FinUnitCOSValue, "Fin", Ans%)
                                'if the facet is not blocked by any other
                                'facet then the subroutine returns with
                                'the variable Ans% equal to 1
IF (Ans% = 1) THEN
                                'the midpoint position pixel is replotted
                                'in the original color
CALL Plot3DPoint(XSpace, YSpace, ZSpace, OldColor)
                                'a facet corner position is plotted as
                                'a point
CALL TransCoordBS(XFinEdgePos(FinNumber%, LeadEdgeLongSegNumber%, 4),
                  YFinEdgePos(FinNumber%, LeadEdgeLongSegNumber%, 4),
                  ZFinEdgePos(LeadEdgeLongSegNumber%, 4), XSpace,
                  YSpace, ZSpace)
CALL Plot3DPoint(XSpace, YSpace, ZSpace, NormalDotProduct * 12 + 3)
                                'lines are drawn between the facet corners
                                'using a display color that indicates the
                                'facets orientation with respect to the
                                'viewer
FOR Corner% = 1 TO 4
    CALL TransCoordBS(XFinEdgePos(FinNumber%, LeadEdgeLongSegNumber%,
                                Corner%), YFinEdgePos(FinNumber%,
                                LeadEdgeLongSegNumber%, Corner%),
                                ZFinEdgePos(LeadEdgeLongSegNumber%, Corner%), XSpace,
                                YSpace, ZSpace)
    CALL Plot3DLine(XSpace, YSpace, ZSpace, NormalDotProduct * 12 + 3)
                                'the facet corner positions are saved for
                                'later transfer to the data storage file
    X(Corner%) = XSpace
    Y(Corner%) = YSpace
    Z(Corner%) = ZSpace
NEXT Corner%

                                'the temperature of the facet is
                                'determined by interpolation and the
                                'data is transferred to the storage file
IF (LeadEdgeLongSegNumber% < NumLeadEdgeLongSeg%) THEN
    CALL AssignFinEdgeTemp(LeadEdgeLongSegNumber%, FinTemp)
    CALL LoadDataFile("Fin ", X(), Y(), Z(), NormalDotProduct, FinLeadEdgeArea,
                      FinTemp, FinEmis)
ELSE
    CALL AssignFinEdgeTemp(LeadEdgeLongSegNumber%, FinTemp)
    CALL LoadDataFile("Fin ", X(), Y(), Z(), NormalDotProduct, FinNonLeadEdgeArea,
                      FinTemp, FinEmis)
END IF

                                'if the view of the facet is blocked by
                                'another facet the midpoint position
                                'pixel is simple returned to its
                                'original color
ELSE
    CALL Plot3DPoint(XSpace, YSpace, ZSpace, OldColor)
END IF
END IF

```

NEXT LeadEdgeLongSegNumber%
 NEXT FinNumber%

'all the aftbody facets are reconsidered

'each transverse aftbody slice is
 'considered

FOR ZSegment% = 0 TO NumLeadEdgeLongSeg% + NumNonLeadEdgeLongSeg% - 1

'the aftbody area between each pair of
 'adjacent fins is considered

FOR FinNumber% = 0 TO NumFins% - 1

'the radial facets within each transverse
 'aftbody slice are considered

FOR AftBodyRadSegNumber% = 0 TO NumAftBodyRadSegPerFin% - 1

'the visibility of a facet to the viewer
 'is determined by first considering the
 'dot product between the facets outwardly
 'pointed normal vector and the unit
 'vector pointing towards the viewer. if
 'this dot product is positive, then the
 'facet may be visible provided that it is
 'not blocked by another facet.

NormalDotProduct = XAftBodyNormal(FinNumber%, AftBodyRadSegNumber%) *
 XViewNormal + YAftBodyNormal(FinNumber%,
 AftBodyRadSegNumber%) * YViewNormal

IF (NormalDotProduct > 0) THEN

'the areal midpoint position of the
 'aftbody facet is calculated in the
 'body coordinate system

CALL CalcAftBodyMidPoint(ZSegment%, FinNumber%, AftBodyRadSegNumber%,
 XMid, YMid, ZMid)

'this midpoint position is transformed to
 'the space coordinate system

CALL TransCoordBS(XMid, YMid, ZMid, XSpace, YSpace, ZSpace)

'the original color of the midpoint
 'position pixel is determined and saved

OldColor = POINT(ZSpace * Scale, YSpace * Scale)

'the aftbody midpoint position is replotted
 'in white to denote which facet is under
 'consideration

CALL Plot3DPoint(XSpace, YSpace, ZSpace, 15)

'all other projectile facets are
 'considered to determine whether any of
 'them will block the viewer's view of
 'this facet

CALL Eclipse(XSpace, YSpace, ZSpace, FinNumber%, FinUnitCOSValue, "AftBody",
 Ans%)

'if the facet is not blocked by any other
 'facet then the subroutine returns with
 'the variable Ans% equal to 1

IF (Ans% = 1) THEN

'the aftbody facet midpoint position
 'pixel is returned to its original color

CALL Plot3DPoint(XSpace, YSpace, ZSpace, OldColor)

'a facet corner position is plotted as
 'a point

CALL TransCoordBS(XAftBodyPos(FinNumber%, AftBodyRadSegNumber%, 4),
 YAftBodyPos(FinNumber%, AftBodyRadSegNumber%, 4),
 ZAftBodyPos(ZSegment%, 4), XSpace, YSpace, ZSpace)

CALL Plot3DPoint(XSpace, YSpace, ZSpace, NormalDotProduct * 12 + 3)

'lines are drawn between the facet corners
 'using a display color that indicates the
 'facets orientation with respect to the
 'viewer

FOR Corner% = 1 TO 4

CALL TransCoordBS(XAftBodyPos(FinNumber%, AftBodyRadSegNumber%,
 Corner%), YAftBodyPos(FinNumber%,

```

                                AftBodyRadSegNumber%, Corner%),
                                ZAftBodyPos(ZSegment%, Corner%), XSpace, YSpace,
                                ZSpace)
CALL Plot3DLine(XSpace, YSpace, ZSpace, NormalDotProduct * 12 + 3)
                                'the facet corner positions are saved for
                                'later transfer to the data storage file

X(Corner%) = XSpace
Y(Corner%) = YSpace
Z(Corner%) = ZSpace
NEXT Corner%

                                'the temperature of the aftbody facet is
                                'determined by interpolation
CALL AssignAftBodyTemp(ZSegment%, AftBodyTemp)
                                'data is transferred to the storage file
CALL LoadDataFile("Aft ", X(), Y(), Z(), NormalDotProduct, AftBodyArea,
                                AftBodyTemp, AftBodyEmis)
                                'if the aftbody facet is blocked by
                                'another facet then the midpoint position
                                'pixel is simply returned to its original
                                'color

ELSE
CALL Plot3DPoint(XSpace, YSpace, ZSpace, OldColor)
END IF
END IF
NEXT AftBodyRadSegNumber%
NEXT FinNumber%
NEXT ZSegment%

                                'the data storage file is terminated
                                'and closed

PRINT #1, "END "
CLOSE #1

                                'a completion statement is output to the
                                'monitor screen

LOCATE 27, 2
PRINT "DONE"

                                'a user terminated do loop is executed to
                                'allow the graphic image to remain on the
                                'monitor screen for possible graphic
                                'capture

DO
  LOOP WHILE INKEY$ = ""

REM $STATIC
SUB AssignAftBodyTemp (ZSegment%, AftBodyTemp)
*****

'THIS SUBROUTINE DETERMINES AFTBODY TEMPERATURES BY LINEARLY INTERPOLATING
'BETWEEN THE PREVIOUSLY DEFINED TEMPERATURES AT THE FRONT AND REAR OF THE
'AFTBODY SECTION
*****

  SHARED NumLeadEdgeLongSeg%, NumNonLeadEdgeLongSeg%
  SHARED AftBodyForwTemp, AftBodyRearTemp

  AftBodyTemp = AftBodyForwTemp + (AftBodyRearTemp - AftBodyForwTemp) * (ZSegment%
  (NumLeadEdgeLongSeg% + NumNonLeadEdgeLongSeg% - 1))

END SUB

SUB AssignBodyTemp (ZSegment%, BodyTemp)

```

```
*****
'THIS SUBROUTINE DETERMINES BODY TEMPERATURES BY LINEARLY INTERPOLATING
'BETWEEN THE PREVIOUSLY DEFINED TEMPERATURES AT THE FRONT AND REAR OF THE
'BODY SECTION
*****
```

```
    SHARED NumBodyLongSeg%, BodyForwTemp, BodyRearTemp
```

```
    BodyTemp = BodyRearTemp + (BodyForwTemp - BodyRearTemp) * ((NumBodyLongSeg% - 1) -
ZSegment%) / (NumBodyLongSeg% - 1)
```

```
END SUB
```

```
SUB AssignFinEdgeTemp (LeadEdgeLongSegNumber%, FinTemp)
```

```
*****
'THIS SUBROUTINE DETERMINES FIN EDGE TEMPERATURES BY LINEARLY INTERPOLATING
'BETWEEN THE PREVIOUSLY DEFINED TEMPERATURES AT THE INNERMOST AND
OUTERMOST
'FIN EDGE POSITIONS
*****
```

```
    SHARED NumLeadEdgeLongSeg%, NumNonLeadEdgeLongSeg%, FinOuterWRTInnerTemp
    SHARED FinLeadTemp, FinTrailTemp
```

```
    IF (LeadEdgeLongSegNumber% < NumLeadEdgeLongSeg%) THEN
        FinTemp = FinLeadTemp + ((LeadEdgeLongSegNumber%) / (NumLeadEdgeLongSeg% - 1)) *
            FinOuterWRTInnerTemp
    ELSE
        FinTemp = FinLeadTemp + FinOuterWRTInnerTemp
    END IF
```

```
END SUB
```

```
SUB AssignFinSideTemp (LeadEdgeLongSegNumber%, FinRadSegNumber%, FinTemp)
```

```
*****
'THIS SUBROUTINE DETERMINES FIN SIDE TEMPERATURES BY LINEARLY INTERPOLATING
'BETWEEN THE PREVIOUSLY DEFINED TEMPERATURES AT THE INNERMOST, OUTERMOST,
'LEADING AND TRAILING EDGE POSITIONS
*****
```

```
    SHARED NumLeadEdgeLongSeg%, NumNonLeadEdgeLongSeg%, NumFinRadSeg%
    SHARED FinOuterWRTInnerTemp, FinLeadTemp, FinTrailTemp
```

```
    FinTemp = FinLeadTemp - ((LeadEdgeLongSegNumber%) / (NumLeadEdgeLongSeg% +
        NumNonLeadEdgeLongSeg% - 1)) * (FinLeadTemp - FinTrailTemp)
    FinTemp = FinTemp + ((FinRadSegNumber%) / (NumFinRadSeg% - 1)) *
        FinOuterWRTInnerTemp
```

```
END SUB
```

```
SUB AssignNoseTemp (ZSegment%, NoseTemp)
```



```
*****
'THIS SUBROUTINE DETERMINES NOSE CONE TEMPERATURES BY LINEARLY INTERPOLATING
'BETWEEN THE PREVIOUSLY DEFINED TEMPERATURES AT THE FRONT AND REAR OF THE
'NOSE CONE
*****
```

```
    SHARED NumNoseConeLongSeg%, NoseForwTemp, NoseRearTemp
```

```
    NoseTemp = NoseRearTemp + (NoseForwTemp - NoseRearTemp) *
                    (((NumNoseConeLongSeg% - 1) - ZSegment%) / (NumNoseConeLongSeg% - 1))
```

```
END SUB
```

```
SUB CalcAftBodyMidPoint (ZSegment%, FinNumber%, AftBodyRadSegNumber%, XMid, YMid,
                        ZMid)
```

```
*****
'THIS SUBROUTINE CALCULATED THE MIDPOINT POSITION OF AN AFTBODY FACET BY
'AVERAGING THE POSITIONS OF THE FACET'S FOUR CORNERS
*****
```

```
    SHARED XAftBodyPos(), YAftBodyPos(), ZAftBodyPos()
```

```
    XMid = 0
    YMid = 0
    ZMid = 0
```

```
    FOR Corner% = 1 TO 4
        XMid = XMid + XAftBodyPos(FinNumber%, AftBodyRadSegNumber%, Corner%) / 4
        YMid = YMid + YAftBodyPos(FinNumber%, AftBodyRadSegNumber%, Corner%) / 4
        ZMid = ZMid + ZAftBodyPos(ZSegment%, Corner%) / 4
    NEXT Corner%
```

```
END SUB
```

```
SUB CalcAftBodyPos
```

```
*****
'THIS SUBROUTINE CALCULATES THE POSITIONS OF THE CORNERS, THE AREA, AND THE
'COMPONENTS OF THE NORMAL VECTOR FOR THE AFTERBODY FACETS.
*****
```

```
    SHARED NumFins%, ThickFin, DeltaZFin, NumLeadEdgeLongSeg%, RadBody
    SHARED NumNonLeadEdgeLongSeg%, NumAftBodyRadSegPerFin%, LengthNoseCone
    SHARED LengthBody, ZAftBodyPos(), XAftBodyPos(), YAftBodyPos()
    SHARED ZAftBodyNormal, XAftBodyNormal(), YAftBodyNormal(), AftBodyArea
```

```

                                'the constant cord length of each facet is
                                'calculated taking into account the
                                'thickness of the fins
    ChordPerAftBodyRadSeg = (2 * 3.14159 * RadBody - NumFins% * ThickFin) / (NumFins% *
                                NumAftBodyRadSegPerFin%)
```

```

                                'the constant area of the afterbody facets
                                'is calculated
    AftBodyArea = ChordPerAftBodyRadSeg * DeltaZFin
```

```

                                'each afterbody facet is considered
                                'starting at the junction between the body
                                'and the afterbody and working rearward to
                                'the projectile end
    FOR ZSegment% = 0 TO NumLeadEdgeLongSeg% + NumNonLeadEdgeLongSeg% - 1
```

```

'ZPosition1 is the more forward facet
'longitudinal position
ZPosition1 = LengthNoseCone + LengthBody + ZSegment% * DeltaZFin
'ZPosition2 is the more rearward facet
'longitudinal position
ZPosition2 = LengthNoseCone + LengthBody + (ZSegment% + 1) * DeltaZFin
'considering the afterbody area between
'each fin in turn
FOR FinNumber% = 0 TO NumFins% - 1
    'the radially oriented facets are
    'considered for each longitudinal slice
    'of each afterbody area
    FOR AftBodyRadSegNumber% = 0 TO NumAftBodyRadSegPerFin% - 1
        'the radial angle from the x axis to the
        'afterbody corner positions is calculated
        AngleAftBodyRadSeg1 = (ThickFin * (FinNumber% + .5) + FinNumber% *
            ChordPerAftBodyRadSeg * NumAftBodyRadSegPerFin% +
            ChordPerAftBodyRadSeg * AftBodyRadSegNumber%) / RadBody
        AngleAftBodyRadSeg2 = (ThickFin * (FinNumber% + .5) + FinNumber% *
            ChordPerAftBodyRadSeg * NumAftBodyRadSegPerFin% +
            ChordPerAftBodyRadSeg * (AftBodyRadSegNumber% + 1)) /
            RadBody
        'the corner positions are calculated
        ZAftBodyPos(ZSegment%, 1) = ZPosition1
        XAftBodyPos(FinNumber%, AftBodyRadSegNumber%, 1) = -RadBody *
            COS(AngleAftBodyRadSeg2)
        YAftBodyPos(FinNumber%, AftBodyRadSegNumber%, 1) = RadBody *
            SIN(AngleAftBodyRadSeg2)
        ZAftBodyPos(ZSegment%, 2) = ZPosition2
        XAftBodyPos(FinNumber%, AftBodyRadSegNumber%, 2) = -RadBody *
            COS(AngleAftBodyRadSeg2)
        YAftBodyPos(FinNumber%, AftBodyRadSegNumber%, 2) = RadBody *
            SIN(AngleAftBodyRadSeg2)
        ZAftBodyPos(ZSegment%, 3) = ZPosition2
        XAftBodyPos(FinNumber%, AftBodyRadSegNumber%, 3) = -RadBody *
            COS(AngleAftBodyRadSeg1)
        YAftBodyPos(FinNumber%, AftBodyRadSegNumber%, 3) = RadBody *
            SIN(AngleAftBodyRadSeg1)
        ZAftBodyPos(ZSegment%, 4) = ZPosition1
        XAftBodyPos(FinNumber%, AftBodyRadSegNumber%, 4) = -RadBody *
            COS(AngleAftBodyRadSeg1)
        YAftBodyPos(FinNumber%, AftBodyRadSegNumber%, 4) = RadBody *
            SIN(AngleAftBodyRadSeg1)
        'the components of the normal vectors
        'are calculated
        ZAftBodyNormal = 0
        XAftBodyNormal(FinNumber%, AftBodyRadSegNumber%) =
            -COS((AngleAftBodyRadSeg1 + AngleAftBodyRadSeg2) / 2)
        YAftBodyNormal(FinNumber%, AftBodyRadSegNumber%) =
            SIN((AngleAftBodyRadSeg1 + AngleAftBodyRadSeg2) / 2)
    NEXT AftBodyRadSegNumber%
NEXT FinNumber%
NEXT ZSegment%
END SUB
SUB CalcBodyPos

```

 'THIS SUBROUTINE CALCULATES THE POSITIONS OF THE CORNERS, THE AREA, AND THE
 'COMPONENTS OF THE NORMAL VECTOR FOR THE BODY FACETS.

'NOTE THAT SYMMETRY ALLOWS THE FOLLOWING SIMPLIFICATIONS:

- ' * THE CORD LENGTH OF ALL THE FACETS WILL BE THE SAME
 - ' * THE Z COMPONENT OF ALL THE FACET BODY NORMALS WILL BE ZERO
 - ' * ALL THE FACET AREAS WILL BE THE SAME
- *****

SHARED LengthBody, DeltaZBody, RadBody, NumBodyRadSeg%
 SHARED ZBodyPos(), XBodyPos(), YBodyPos(), BodyArea
 SHARED ZBodyNormal, XBodyNormal(), YBodyNormal(), NumBodyLongSeg%
 SHARED LengthNoseCone

MaxBodyChordLength = 2 * 3.14159 * RadBody / NumBodyRadSeg%
 'constant chord length of each facet is
 'calculated
 'for the body facets the value of theta
 'is zero.

TanTheta = 0
 CosTheta = 1
 SinTheta = 0

FOR ZSegment% = 0 TO NumBodyLongSeg% - 1
 'each body facet is considered starting at
 'the junction between the nose and the
 'body and working back towards the
 'junction with the aft body

ZPosition1 = ZSegment% * DeltaZBody
 'ZPosition1 is the more forward facet
 'longitudinal position

ZPosition2 = (ZSegment% + 1) * DeltaZBody
 'ZPosition2 is the more rearward facet
 'longitudinal position

FOR CordSegment% = 0 TO NumBodyRadSeg% - 1
 'the radially oriented facets are
 'considered for each longitudinal slice

'the facet corner positions are calculated

ZBodyPos(ZSegment%, 1) = ZPosition1 + LengthNoseCone
 XBodyPos(CordSegment%, 1) = -RadBody * COS(2 * 3.14159 * (CordSegment% + .5) /
 NumBodyRadSeg%)

YBodyPos(CordSegment%, 1) = RadBody * SIN(2 * 3.14159 * (CordSegment% + .5) /
 NumBodyRadSeg%)

ZBodyPos(ZSegment%, 2) = ZPosition2 + LengthNoseCone
 XBodyPos(CordSegment%, 2) = -RadBody * COS(2 * 3.14159 * (CordSegment% + .5) /
 NumBodyRadSeg%)

YBodyPos(CordSegment%, 2) = RadBody * SIN(2 * 3.14159 * (CordSegment% + .5) /
 NumBodyRadSeg%)

ZBodyPos(ZSegment%, 3) = ZPosition2 + LengthNoseCone
 XBodyPos(CordSegment%, 3) = -RadBody * COS(2 * 3.14159 * (CordSegment% - .5) /
 NumBodyRadSeg%)

YBodyPos(CordSegment%, 3) = RadBody * SIN(2 * 3.14159 * (CordSegment% - .5) /
 NumBodyRadSeg%)

ZBodyPos(ZSegment%, 4) = ZPosition1 + LengthNoseCone
 XBodyPos(CordSegment%, 4) = -RadBody * COS(2 * 3.14159 * (CordSegment% - .5) /
 NumBodyRadSeg%)

YBodyPos(CordSegment%, 4) = RadBody * SIN(2 * 3.14159 * (CordSegment% - .5) /
 NumBodyRadSeg%)

BodyArea = MaxBodyChordLength * DeltaZBody
 'the facet area is calculated

'the facet normal vector components are
 'calculated

```

ZBodyNormal = 0
XBodyNormal(CordSegment%) = -CosTheta * COS(2 * 3.14159 * CordSegment% /
                                     NumBodyRadSeg%)
YBodyNormal(CordSegment%) = CosTheta * SIN(2 * 3.14159 * CordSegment% /
                                     NumBodyRadSeg%)
NEXT CordSegment%
NEXT ZSegment%

```

END SUB

SUB CalcBoxExtremes

 'THIS SUBROUTINE DETERMINES THE EXTREME PROJECTILE POSITIONS SO THAT A
 'PROPERLY SIZED GRAPHICS SCREEN CAN BE INITIALIZED

```

SHARED ZNoseConePos(), XNoseConePos(), YNoseConePos(), NumNoseConeLongSeg%
SHARED NumNoseConeRadSeg%, ZBoxMin, ZBoxMax, XBoxMin, XBoxMax, YBoxMin
SHARED YBoxMax, ZBodyPos(), XBodyPos(), YBodyPos()
SHARED NumBodyLongSeg%, NumBodyRadSeg%, ZFinEdgePos(), YFinEdgePos()
SHARED XFinEdgePos(), NumFins%, NumLeadEdgeLongSeg%
SHARED NumNonLeadEdgeLongSeg%

```

```

ZBoxMin = 1E+10
ZBoxMax = -1E+10
XBoxMin = 1E+10
XBoxMax = -1E+10
YBoxMin = 1E+10
YBoxMax = -1E+10

```

'checking all the nose cone positions

```

FOR ZSegment% = 0 TO NumNoseConeLongSeg% - 1
  FOR CordSegment% = 0 TO NumNoseConeRadSeg% - 1
    FOR Corner% = 1 TO 4
      IF (ZNoseConePos(ZSegment%, Corner%) > ZBoxMax) THEN ZBoxMax =
        ZNoseConePos(ZSegment%, Corner%)
      IF (ZNoseConePos(ZSegment%, Corner%) < ZBoxMin) THEN ZBoxMin =
        ZNoseConePos(ZSegment%, Corner%)
      IF (XNoseConePos(ZSegment%, CordSegment%, Corner%) > XBoxMax) THEN
        XBoxMax = XNoseConePos(ZSegment%, CordSegment%,
        Corner%)
      IF (XNoseConePos(ZSegment%, CordSegment%, Corner%) < XBoxMin) THEN
        XBoxMin = XNoseConePos(ZSegment%, CordSegment%, Corner%)
      IF (YNoseConePos(ZSegment%, CordSegment%, Corner%) > YBoxMax) THEN
        YBoxMax = YNoseConePos(ZSegment%, CordSegment%, Corner%)
      IF (YNoseConePos(ZSegment%, CordSegment%, Corner%) < YBoxMin) THEN
        YBoxMin = YNoseConePos(ZSegment%, CordSegment%, Corner%)
    NEXT Corner%
  NEXT CordSegment%
NEXT ZSegment%

```

'checking all the body positions

```

FOR ZSegment% = 0 TO NumBodyLongSeg% - 1
  FOR CordSegment% = 0 TO NumBodyRadSeg% - 1
    FOR Corner% = 1 TO 4
      IF (ZBodyPos(ZSegment%, Corner%) > ZBoxMax) THEN ZBoxMax =
        ZBodyPos(ZSegment%, Corner%)
      IF (ZBodyPos(ZSegment%, Corner%) < ZBoxMin) THEN ZBoxMin =
        ZBodyPos(ZSegment%, Corner%)
      IF (XBodyPos(CordSegment%, Corner%) > XBoxMax) THEN XBoxMax =
        XBodyPos(CordSegment%, Corner%)
      IF (XBodyPos(CordSegment%, Corner%) < XBoxMin) THEN XBoxMin =
        XBodyPos(CordSegment%, Corner%)
      IF (YBodyPos(CordSegment%, Corner%) > YBoxMax) THEN YBoxMax =
        YBodyPos(CordSegment%, Corner%)
    NEXT Corner%
  NEXT CordSegment%
NEXT ZSegment%

```

```

        IF (YBodyPos(CordSegment%, Corner%) < YBoxMin) THEN YBoxMin =
            YBodyPos(CordSegment%, Corner%)
        NEXT Corner%
    NEXT CordSegment%
    NEXT ZSegment%

'checking all the fin positions
FOR FinNumber% = 0 TO NumFins% - 1
    FOR ZSegment% = 0 TO NumLeadEdgeLongSeg% + NumNonLeadEdgeLongSeg% - 1
        FOR Corner% = 1 TO 4
            IF (ZFinEdgePos(ZSegment%, Corner%) > ZBoxMax) THEN ZBoxMax =
                ZFinEdgePos(ZSegment%, Corner%)
            IF (ZFinEdgePos(ZSegment%, Corner%) < ZBoxMin) THEN ZBoxMin =
                ZFinEdgePos(ZSegment%, Corner%)
            IF (XFinEdgePos(FinNumber%, ZSegment%, Corner%) > XBoxMax) THEN XBoxMax =
                XFinEdgePos(FinNumber%, ZSegment%, Corner%)
            IF (XFinEdgePos(FinNumber%, ZSegment%, Corner%) < XBoxMin) THEN XBoxMin =
                XFinEdgePos(FinNumber%, ZSegment%, Corner%)
            IF (YFinEdgePos(FinNumber%, ZSegment%, Corner%) > YBoxMax) THEN YBoxMax =
                YFinEdgePos(FinNumber%, ZSegment%, Corner%)
            IF (YFinEdgePos(FinNumber%, ZSegment%, Corner%) < YBoxMin) THEN YBoxMin =
                YFinEdgePos(FinNumber%, ZSegment%, Corner%)
        NEXT Corner%
    NEXT ZSegment%
NEXT FinNumber%

'it is assumed that an aftbody position
'will never be at an extreme location

END SUB

SUB CalcEulerElem
*****

'THIS SUBROUTINE CALCULATES THE MATRIX ELEMENTS THAT ARE NECESSARY TO
'TRANSFORM BETWEEN PROJECTILE AND SPACE COORDINATES
*****

    SHARED Euler(), E()

    E(1, 1) = COS(Euler(1)) * COS(Euler(3)) - SIN(Euler(1)) * COS(Euler(2)) * SIN(Euler(3))
    E(1, 2) = -COS(Euler(1)) * SIN(Euler(3)) - SIN(Euler(1)) * COS(Euler(2)) * COS(Euler(3))
    E(1, 3) = SIN(Euler(1)) * SIN(Euler(2))
    E(2, 1) = SIN(Euler(1)) * COS(Euler(3)) + COS(Euler(1)) * COS(Euler(2)) * SIN(Euler(3))
    E(2, 2) = -SIN(Euler(1)) * SIN(Euler(3)) + COS(Euler(1)) * COS(Euler(2)) * COS(Euler(3))
    E(2, 3) = -COS(Euler(1)) * SIN(Euler(2))
    E(3, 1) = SIN(Euler(2)) * SIN(Euler(3))
    E(3, 2) = SIN(Euler(2)) * COS(Euler(3))
    E(3, 3) = COS(Euler(2))

END SUB

SUB CalcFinEdgeMidPoint (FinNumber%, LeadEdgeLongSegNumber%, XMid, YMid, ZMid)
*****

'THIS SUBROUTINE CALCULATED THE MIDPOINT POSITIONS OF FIN EDGE FACETS BY
' AVERAGING THE POSITIONS OF THE FACET'S FOUR CORNERS
*****

    SHARED XFinEdgePos(), YFinEdgePos(), ZFinEdgePos()

    XMid = 0
    YMid = 0
    ZMid = 0
    FOR Corner% = 1 TO 4

```

```

XMid = XMid + XFinEdgePos(FinNumber%, LeadEdgeLongSegNumber%, Corner%) / 4
YMid = YMid + YFinEdgePos(FinNumber%, LeadEdgeLongSegNumber%, Corner%) / 4
ZMid = ZMid + ZFinEdgePos(LeadEdgeLongSegNumber%, Corner%) / 4
NEXT Corner%

```

END SUB

SUB CalcFinPos

 'THIS SUBROUTINE CALCULATES THE POSITIONS OF THE CORNERS, THE AREA, AND THE
 'COMPONENTS OF THE NORMAL VECTOR FOR THE FIN FACETS.

'NOTE THAT SYMMETRY ALLOWS THE FOLLOWING SIMPLIFICATIONS:

- ' * ALL THE LEADING EDGE FACETS WILL HAVE THE SAME Z COMPONENT OF THE
 ' NORMAL VECTOR
- ' * ALL THE LEADING EDGE FACETS HAVE THE SAME AREA
- ' * ALL THE NON-LEADING EDGE FACETS HAVE A NORMAL VECTOR Z COMPONENT
 ' OF ZERO
- ' * ALL THE NON-LEADING EDGE FACETS HAVE THE SAME AREA
- ' * ALL THE SIDE FACETS HAVE A NORMAL VECTOR Z COMPONENT OF ZERO
- ' * ALL THE SIDE FACETS ON ONE SIDE OF A GIVEN FIN HAVE THE SAME NORMAL
 ' VECTOR X AND Y COMPONENTS
- ' * ALL THE SIDE FACETS IN THE NON-LEADING EDGE AREA OF THE FIN HAVE THE
 ' SAME AREA

 SHARED NumFins%, ThickFin, LengthLeadEdgeFin, DeltaZFin
 SHARED NumLeadEdgeLongSeg%, HeightFin, NumNonLeadEdgeLongSeg%
 SHARED DeltaRadFin, NumFinRadSeg%, LengthNoseCone, LengthBody, RadBody
 SHARED ZFinEdgePos(), YFinEdgePos(), XFinEdgePos()
 SHARED ZFinPos(), YFinPos(), XFinPos()
 SHARED ZFinLeadEdgeNormal, XFinLeadEdgeNormal(), YFinLeadEdgeNormal()
 SHARED ZFinNonLeadEdgeNormal, XFinNonLeadEdgeNormal(), YFinNonLeadEdgeNormal()
 SHARED ZFinSideNormal, XFinSideNormal(), YFinSideNormal(), FinLeadEdgeArea
 SHARED FinNonLeadEdgeArea, FinLeadSideArea(), FinNonLeadSideArea
 'the angle that the fin leading edge makes
 'with the projectile body is considered

$$\text{FinLeadEdgeSIN} = \text{HeightFin} / \text{SQR}((\text{LengthLeadEdgeFin}^2) + (\text{HeightFin}^2))$$

$$\text{FinLeadEdgeCOS} = \text{LengthLeadEdgeFin} / \text{SQR}((\text{LengthLeadEdgeFin}^2) + (\text{HeightFin}^2))$$

 'the constant area of the fin leading edge
 'facets is calculated

$$\text{FinLeadEdgeArea} = \text{ThickFin} * \text{DeltaZFin} / \text{FinLeadEdgeCOS}$$

 'the constant area of the fin non-leading
 'edge edge facets is calculated

$$\text{FinNonLeadEdgeArea} = \text{ThickFin} * \text{DeltaZFin}$$

 'the constant area of the fin side facets
 'that are not associated with a leading
 'edge longitudinal position is calculated

$$\text{FinNonLeadSideArea} = \text{DeltaZFin} * \text{DeltaRadFin}$$

 'each fin is considered in turn
 FOR FinNumber% = 0 TO NumFins% - 1
 'the angle is considered between the x
 'axis and a vector that is normal to the
 'projectile center line and is in the
 'plane of the fin under consideration

$$\text{FinRadSIN} = \text{SIN}(2 * 3.14159 * \text{FinNumber\%} / \text{NumFins\%})$$

```

FinRadCOS = COS(2 * 3.14159 * FinNumber% / NumFins%)
' the components of the fins extension
' away from the central plane of the fin
' due to the fin's thickness are calculated
FinThickSINFactor = (ThickFin / 2) * SIN(2 * 3.14159 * FinNumber% / NumFins%)
FinThickCOSFactor = (ThickFin / 2) * COS(2 * 3.14159 * FinNumber% / NumFins%)
' the components of the normals of the fin
' side facets are calculated taking into
' account the fact that side facets can
' be paired by which "side" of the fin they
' are located on.

ZFinSideNormal = 0
XFinSideNormal(FinNumber%, 1) = FinRadSIN
XFinSideNormal(FinNumber%, 2) = -FinRadSIN
YFinSideNormal(FinNumber%, 1) = FinRadCOS
YFinSideNormal(FinNumber%, 2) = -FinRadCOS

' starting at the front of the fin the
' corner positions, orientations, and areas
' are calculated for the longitudinal
' positions corresponding to the leading
' edge
FOR LeadEdgeLongSegNumber% = 0 TO NumLeadEdgeLongSeg% - 1
' the leading edge facets are considered
' for this leading edge longitudinal
' position
ZPosition1 = LengthNoseCone + LengthBody + LeadEdgeLongSegNumber% * DeltaZFin
ZPosition2 = LengthNoseCone + LengthBody + (LeadEdgeLongSegNumber% + 1) *
DeltaZFin
' the facet corner positions are calculated
ZFinEdgePos(LeadEdgeLongSegNumber%, 1) = ZPosition1
XFinEdgePos(FinNumber%, LeadEdgeLongSegNumber%, 1) = -(RadBody + HeightFin *
LeadEdgeLongSegNumber% / NumLeadEdgeLongSeg%) *
FinRadCOS + FinThickSINFactor
YFinEdgePos(FinNumber%, LeadEdgeLongSegNumber%, 1) = (RadBody + HeightFin *
LeadEdgeLongSegNumber% / NumLeadEdgeLongSeg%) *
FinRadSIN + FinThickCOSFactor
ZFinEdgePos(LeadEdgeLongSegNumber%, 2) = ZPosition2
XFinEdgePos(FinNumber%, LeadEdgeLongSegNumber%, 2) = -(RadBody + HeightFin *
(LeadEdgeLongSegNumber% + 1) / NumLeadEdgeLongSeg%) *
FinRadCOS + FinThickSINFactor
YFinEdgePos(FinNumber%, LeadEdgeLongSegNumber%, 2) = (RadBody + HeightFin *
(LeadEdgeLongSegNumber% + 1) / NumLeadEdgeLongSeg%) *
FinRadSIN + FinThickCOSFactor
ZFinEdgePos(LeadEdgeLongSegNumber%, 3) = ZPosition2
XFinEdgePos(FinNumber%, LeadEdgeLongSegNumber%, 3) = -(RadBody + HeightFin *
(LeadEdgeLongSegNumber% + 1) / NumLeadEdgeLongSeg%) *
FinRadCOS - FinThickSINFactor
YFinEdgePos(FinNumber%, LeadEdgeLongSegNumber%, 3) = (RadBody + HeightFin *
(LeadEdgeLongSegNumber% + 1) / NumLeadEdgeLongSeg%) *
FinRadSIN - FinThickCOSFactor
ZFinEdgePos(LeadEdgeLongSegNumber%, 4) = ZPosition1
XFinEdgePos(FinNumber%, LeadEdgeLongSegNumber%, 4) = -(RadBody + HeightFin *
LeadEdgeLongSegNumber% / NumLeadEdgeLongSeg%) *
FinRadCOS - FinThickSINFactor
YFinEdgePos(FinNumber%, LeadEdgeLongSegNumber%, 4) = (RadBody + HeightFin *
LeadEdgeLongSegNumber% / NumLeadEdgeLongSeg%) *
FinRadSIN - FinThickCOSFactor
' the facet normal vector components are
' calculated
ZFinLeadEdgeNormal = -FinLeadEdgeSIN
XFinLeadEdgeNormal(FinNumber%) = -FinLeadEdgeCOS * FinRadCOS
YFinLeadEdgeNormal(FinNumber%) = FinLeadEdgeCOS * FinRadSIN
' the facet area is calculated
FinLeadSideArea(LeadEdgeLongSegNumber%) = .5 * (LeadEdgeLongSegNumber% + 1) *
DeltaZFin * HeightFin * ((LeadEdgeLongSegNumber% + 1) /
NumLeadEdgeLongSeg%) - (.5 * (LeadEdgeLongSegNumber%) *

```

```

DeltaZFin * HeightFin * ((LeadEdgeLongSegNumber% /
NumLeadEdgeLongSeg%))
the side facets are considered for this
leading edge longitudinal position
FOR LeadEdgeRadSegNumber% = 0 TO NumFinRadSeg% - 1
the facet corner positions are calculated
ZFinPos(LeadEdgeLongSegNumber%, 1) = ZPosition1
XFinPos(FinNumber%, LeadEdgeLongSegNumber%, LeadEdgeRadSegNumber%, 1, 1) =
-(RadBody + HeightFin * (LeadEdgeLongSegNumber% /
NumLeadEdgeLongSeg%) * (LeadEdgeRadSegNumber% /
NumFinRadSeg%)) * FinRadCOS + FinThickSINFactor
YFinPos(FinNumber%, LeadEdgeLongSegNumber%, LeadEdgeRadSegNumber%, 1, 1) =
(RadBody + HeightFin * (LeadEdgeLongSegNumber% /
NumLeadEdgeLongSeg%) * (LeadEdgeRadSegNumber% /
NumFinRadSeg%)) * FinRadSIN +
FinThickCOSFactor
ZFinPos(LeadEdgeLongSegNumber%, 2) = ZPosition1
XFinPos(FinNumber%, LeadEdgeLongSegNumber%, LeadEdgeRadSegNumber%, 1, 2) =
-(RadBody + HeightFin * (LeadEdgeLongSegNumber% /
NumLeadEdgeLongSeg%) * ((LeadEdgeRadSegNumber% + 1) /
NumFinRadSeg%)) * FinRadCOS + FinThickSINFactor
YFinPos(FinNumber%, LeadEdgeLongSegNumber%, LeadEdgeRadSegNumber%, 1, 2) =
(RadBody + HeightFin * (LeadEdgeLongSegNumber% /
NumLeadEdgeLongSeg%) * ((LeadEdgeRadSegNumber% + 1) /
NumFinRadSeg%)) * FinRadSIN +
FinThickCOSFactor
ZFinPos(LeadEdgeLongSegNumber%, 3) = ZPosition2
XFinPos(FinNumber%, LeadEdgeLongSegNumber%, LeadEdgeRadSegNumber%, 1, 3) =
-(RadBody + HeightFin * ((LeadEdgeLongSegNumber% + 1) /
NumLeadEdgeLongSeg%) * ((LeadEdgeRadSegNumber% + 1) /
NumFinRadSeg%)) * FinRadCOS + FinThickSINFactor
YFinPos(FinNumber%, LeadEdgeLongSegNumber%, LeadEdgeRadSegNumber%, 1, 3) =
(RadBody + HeightFin * ((LeadEdgeLongSegNumber% + 1) /
NumLeadEdgeLongSeg%) * ((LeadEdgeRadSegNumber% + 1) /
NumFinRadSeg%)) * FinRadSIN + FinThickCOSFactor
ZFinPos(LeadEdgeLongSegNumber%, 4) = ZPosition2
XFinPos(FinNumber%, LeadEdgeLongSegNumber%, LeadEdgeRadSegNumber%, 1, 4) =
-(RadBody + HeightFin * ((LeadEdgeLongSegNumber% + 1) /
NumLeadEdgeLongSeg%) * (LeadEdgeRadSegNumber% /
NumFinRadSeg%)) * FinRadCOS + FinThickSINFactor
YFinPos(FinNumber%, LeadEdgeLongSegNumber%, LeadEdgeRadSegNumber%, 1, 4) =
(RadBody + HeightFin * ((LeadEdgeLongSegNumber% + 1) /
NumLeadEdgeLongSeg%) * (LeadEdgeRadSegNumber% /
NumFinRadSeg%)) * FinRadSIN + FinThickCOSFactor
XFinPos(FinNumber%, LeadEdgeLongSegNumber%, LeadEdgeRadSegNumber%, 2, 1) =
-(RadBody + HeightFin * (LeadEdgeLongSegNumber% /
NumLeadEdgeLongSeg%) * (LeadEdgeRadSegNumber% /
NumFinRadSeg%)) * FinRadCOS - FinThickSINFactor
YFinPos(FinNumber%, LeadEdgeLongSegNumber%, LeadEdgeRadSegNumber%, 2, 1) =
(RadBody + HeightFin * (LeadEdgeLongSegNumber% /
NumLeadEdgeLongSeg%) * (LeadEdgeRadSegNumber% /
NumFinRadSeg%)) * FinRadSIN -
FinThickCOSFactor
XFinPos(FinNumber%, LeadEdgeLongSegNumber%, LeadEdgeRadSegNumber%, 2, 2) =
-(RadBody + HeightFin * (LeadEdgeLongSegNumber% /
NumLeadEdgeLongSeg%) * ((LeadEdgeRadSegNumber% + 1) /
NumFinRadSeg%)) * FinRadCOS - FinThickSINFactor
YFinPos(FinNumber%, LeadEdgeLongSegNumber%, LeadEdgeRadSegNumber%, 2, 2) =
(RadBody + HeightFin * (LeadEdgeLongSegNumber% /
NumLeadEdgeLongSeg%) * ((LeadEdgeRadSegNumber% + 1) /
NumFinRadSeg%)) * FinRadSIN -
FinThickCOSFactor
XFinPos(FinNumber%, LeadEdgeLongSegNumber%, LeadEdgeRadSegNumber%, 2, 3) =
-(RadBody + HeightFin * ((LeadEdgeLongSegNumber% + 1) /
NumLeadEdgeLongSeg%) * ((LeadEdgeRadSegNumber% + 1) /
NumFinRadSeg%)) * FinRadCOS - FinThickSINFactor
YFinPos(FinNumber%, LeadEdgeLongSegNumber%, LeadEdgeRadSegNumber%, 2, 3) =
(RadBody + HeightFin * ((LeadEdgeLongSegNumber% + 1) /
NumLeadEdgeLongSeg%) * ((LeadEdgeRadSegNumber% + 1) /
NumFinRadSeg%)) * FinRadSIN - FinThickCOSFactor

```



```

      XFinPos(FinNumber%, LeadEdgeLongSegNumber%, LeadEdgeRadSegNumber%, 2, 4) =
      -(RadBody + HeightFin * ((LeadEdgeLongSegNumber% + 1) /
      NumLeadEdgeLongSeg%) * (LeadEdgeRadSegNumber% /
      NumFinRadSeg%)) * FinRadCOS - FinThickSINFactor
      YFinPos(FinNumber%, LeadEdgeLongSegNumber%, LeadEdgeRadSegNumber%, 2, 4) =
      (RadBody + HeightFin * ((LeadEdgeLongSegNumber% + 1) /
      NumLeadEdgeLongSeg%) * (LeadEdgeRadSegNumber% /
      NumFinRadSeg%)) * FinRadSIN - FinThickCOSFactor
      NEXT LeadEdgeRadSegNumber%
      NEXT LeadEdgeLongSegNumber%

      'starting at the front of the non-leading
      'edge portion of the fin the corner
      'positions, orientations, and areas are
      'calculated for the longitudinal positions
      'corresponding to the non-leading edge.
      FOR NonLeadEdgeLongSegNumber% = NumLeadEdgeLongSeg% TO
      (NumLeadEdgeLongSeg% + NumNonLeadEdgeLongSeg% - 1)
      'the non-leading edge facets are
      'considered for this non-leading edge
      'longitudinal position
      ZPosition1 = LengthNoseCone + LengthBody + NonLeadEdgeLongSegNumber% *
      DeltaZFin
      ZPosition2 = LengthNoseCone + LengthBody + (NonLeadEdgeLongSegNumber% + 1) *
      DeltaZFin
      'the facet corner positions are calculated
      ZFinEdgePos(NonLeadEdgeLongSegNumber%, 1) = ZPosition1
      XFinEdgePos(FinNumber%, NonLeadEdgeLongSegNumber%, 1) = -(RadBody + HeightFin) *
      FinRadCOS + FinThickSINFactor
      YFinEdgePos(FinNumber%, NonLeadEdgeLongSegNumber%, 1) = (RadBody + HeightFin) *
      FinRadSIN + FinThickCOSFactor
      ZFinEdgePos(NonLeadEdgeLongSegNumber%, 2) = ZPosition2
      XFinEdgePos(FinNumber%, NonLeadEdgeLongSegNumber%, 2) = -(RadBody + HeightFin) *
      FinRadCOS + FinThickSINFactor
      YFinEdgePos(FinNumber%, NonLeadEdgeLongSegNumber%, 2) = (RadBody + HeightFin) *
      FinRadSIN + FinThickCOSFactor
      ZFinEdgePos(NonLeadEdgeLongSegNumber%, 3) = ZPosition2
      XFinEdgePos(FinNumber%, NonLeadEdgeLongSegNumber%, 3) = -(RadBody + HeightFin) *
      FinRadCOS - FinThickSINFactor
      YFinEdgePos(FinNumber%, NonLeadEdgeLongSegNumber%, 3) = (RadBody + HeightFin) *
      FinRadSIN - FinThickCOSFactor
      ZFinEdgePos(NonLeadEdgeLongSegNumber%, 4) = ZPosition1
      XFinEdgePos(FinNumber%, NonLeadEdgeLongSegNumber%, 4) = -(RadBody + HeightFin) *
      FinRadCOS - FinThickSINFactor
      YFinEdgePos(FinNumber%, NonLeadEdgeLongSegNumber%, 4) = (RadBody + HeightFin) *
      FinRadSIN - FinThickCOSFactor
      'the facet normal vector components
      'are calculated
      ZFinNonLeadEdgeNormal = 0
      XFinNonLeadEdgeNormal(FinNumber%) = -FinRadCOS
      YFinNonLeadEdgeNormal(FinNumber%) = FinRadSIN
      'the side facets are considered for this
      'non-leading edge longitudinal position
      FOR NonLeadEdgeRadSegNumber% = 0 TO NumFinRadSeg% - 1
      'the facet corner positions are calculated
      ZFinPos(NonLeadEdgeLongSegNumber%, 1) = ZPosition1
      XFinPos(FinNumber%, NonLeadEdgeLongSegNumber%, NonLeadEdgeRadSegNumber%,
      1, 1) = -(RadBody + HeightFin * NonLeadEdgeRadSegNumber% /
      NumFinRadSeg%) * FinRadCOS + FinThickSINFactor
      YFinPos(FinNumber%, NonLeadEdgeLongSegNumber%, NonLeadEdgeRadSegNumber%,
      1, 1) = (RadBody + HeightFin * NonLeadEdgeRadSegNumber% /
      NumFinRadSeg%) * FinRadSIN + FinThickCOSFactor
      ZFinPos(NonLeadEdgeLongSegNumber%, 2) = ZPosition1
      XFinPos(FinNumber%, NonLeadEdgeLongSegNumber%, NonLeadEdgeRadSegNumber%,
      1, 2) = -(RadBody + HeightFin * (NonLeadEdgeRadSegNumber% + 1) /
      NumFinRadSeg%) * FinRadCOS + FinThickSINFactor
      YFinPos(FinNumber%, NonLeadEdgeLongSegNumber%, NonLeadEdgeRadSegNumber%,

```

```

1, 2) = (RadBody + HeightFin * (NonLeadEdgeRadSegNumber% + 1) /
NumFinRadSeg%) * FinRadSIN + FinThickCOSFactor
ZFinPos(NonLeadEdgeLongSegNumber%, 3) = ZPosition2
XFinPos(FinNumber%, NonLeadEdgeLongSegNumber%, NonLeadEdgeRadSegNumber%,
1, 3) = -(RadBody + HeightFin * (NonLeadEdgeRadSegNumber% + 1) /
NumFinRadSeg%) * FinRadCOS + FinThickSINFactor
YFinPos(FinNumber%, NonLeadEdgeLongSegNumber%, NonLeadEdgeRadSegNumber%,
1, 3) = (RadBody + HeightFin * (NonLeadEdgeRadSegNumber% + 1) /
NumFinRadSeg%) * FinRadSIN + FinThickCOSFactor
ZFinPos(NonLeadEdgeLongSegNumber%, 4) = ZPosition2
XFinPos(FinNumber%, NonLeadEdgeLongSegNumber%, NonLeadEdgeRadSegNumber%,
1, 4) = -(RadBody + HeightFin * NonLeadEdgeRadSegNumber% /
NumFinRadSeg%) * FinRadCOS + FinThickSINFactor
YFinPos(FinNumber%, NonLeadEdgeLongSegNumber%, NonLeadEdgeRadSegNumber%,
1, 4) = (RadBody + HeightFin * NonLeadEdgeRadSegNumber% /
NumFinRadSeg%) * FinRadSIN + FinThickCOSFactor
XFinPos(FinNumber%, NonLeadEdgeLongSegNumber%, NonLeadEdgeRadSegNumber%,
2, 1) = -(RadBody + HeightFin * NonLeadEdgeRadSegNumber% /
NumFinRadSeg%) * FinRadCOS - FinThickSINFactor
YFinPos(FinNumber%, NonLeadEdgeLongSegNumber%, NonLeadEdgeRadSegNumber%,
2, 1) = (RadBody + HeightFin * NonLeadEdgeRadSegNumber% /
NumFinRadSeg%) * FinRadSIN - FinThickCOSFactor
XFinPos(FinNumber%, NonLeadEdgeLongSegNumber%, NonLeadEdgeRadSegNumber%,
2, 2) = -(RadBody + HeightFin * (NonLeadEdgeRadSegNumber% + 1) /
NumFinRadSeg%) * FinRadCOS - FinThickSINFactor
YFinPos(FinNumber%, NonLeadEdgeLongSegNumber%, NonLeadEdgeRadSegNumber%,
2, 2) = (RadBody + HeightFin * (NonLeadEdgeRadSegNumber% + 1) /
NumFinRadSeg%) * FinRadSIN - FinThickCOSFactor
XFinPos(FinNumber%, NonLeadEdgeLongSegNumber%, NonLeadEdgeRadSegNumber%,
2, 3) = -(RadBody + HeightFin * (NonLeadEdgeRadSegNumber% + 1) /
NumFinRadSeg%) * FinRadCOS - FinThickSINFactor
YFinPos(FinNumber%, NonLeadEdgeLongSegNumber%, NonLeadEdgeRadSegNumber%,
2, 3) = (RadBody + HeightFin * (NonLeadEdgeRadSegNumber% + 1) /
NumFinRadSeg%) * FinRadSIN - FinThickCOSFactor
XFinPos(FinNumber%, NonLeadEdgeLongSegNumber%, NonLeadEdgeRadSegNumber%,
2, 4) = -(RadBody + HeightFin * NonLeadEdgeRadSegNumber% /
NumFinRadSeg%) * FinRadCOS - FinThickSINFactor
YFinPos(FinNumber%, NonLeadEdgeLongSegNumber%, NonLeadEdgeRadSegNumber%,
2, 4) = (RadBody + HeightFin * NonLeadEdgeRadSegNumber% /
NumFinRadSeg%) * FinRadSIN - FinThickCOSFactor
NEXT NonLeadEdgeRadSegNumber%
NEXT NonLeadEdgeLongSegNumber%
NEXT FinNumber%

```

END SUB

SUB CalcFinSideMidPoint (FinNumber%, LeadEdgeLongSegNumber%, FinRadSegNumber%,
SideNumber%, XMid, YMid, ZMid)

THIS SUBROUTINE CALCULATED THE MIDPOINT POSITIONS OF FIN SIDE FACETS BY
'AVERAGING THE POSITIONS OF THE FACET'S FOUR CORNERS

SHARED XFinPos(), YFinPos(), ZFinPos()

XMid = 0
YMid = 0
ZMid = 0

FOR Corner% = 1 TO 4

XMid = XMid + XFinPos(FinNumber%, LeadEdgeLongSegNumber%, FinRadSegNumber%,
SideNumber%, Corner%) / 4

YMid = YMid + YFinPos(FinNumber%, LeadEdgeLongSegNumber%, FinRadSegNumber%,

```

SideNumber%, Corner%) / 4
ZMid = ZMid + ZFinPos(LeadEdgeLongSegNumber%, Corner%) / 4
NEXT Corner%

```

END SUB

SUB CalcNoseConePos

'THIS SUBROUTINE CALCULATES THE POSITIONS OF THE CORNERS, THE AREA, AND THE
'COMPONENTS OF THE NORMAL VECTOR FOR THE NOSE CONE FACETS.

'NOTE THAT SYMMETRY ALLOWS THE FOLLOWING SIMPLIFICATION:

' * THE Z COMPONENT OF ALL THE FACET NORMAL VECTORS WILL BE THE SAME

```

SHARED LengthNoseCone, DeltaZNoseCone, NumNoseConeLongSeg%, RadNoseCone
SHARED NumNoseConeRadSeg%, ZNoseConePos(), XNoseConePos(), YNoseConePos()
SHARED NoseConeArea(), ZNoseConeNormal, XNoseConeNormal()
SHARED YNoseConeNormal()

```

'the radial segment cord is calculated at
'the base (or largest diameter) of the
'nose cone

```

MaxNoseConeChordLength = 2 * 3.14159 * RadNoseCone / NumNoseConeRadSeg%

```

'theta is the angle between the center
'line of the projectile and the surface
'of the nose cone

```

TanTheta = RadNoseCone / LengthNoseCone
CosTheta = LengthNoseCone / SQR((RadNoseCone ^ 2) + (LengthNoseCone ^ 2))
SinTheta = RadNoseCone / SQR((RadNoseCone ^ 2) + (LengthNoseCone ^ 2))

```

'each nose cone facet is considered
'starting at the tip and working towards
'the base

```

FOR ZSegment% = 0 TO NumNoseConeLongSeg% - 1

```

'ZPosition1 is the more forward facet
'longitudinal position

```

ZPosition1 = ZSegment% * DeltaZNoseCone

```

'ZPosition2 is the more rearward facet
'longitudinal position

```

ZPosition2 = (ZSegment% + 1) * DeltaZNoseCone

```

'the radially oriented facets are
'considered for each longitudinal slice

```

FOR CordSegment% = 0 TO NumNoseConeRadSeg% - 1

```

'the facet corner positions are calculated

```

ZNoseConePos(ZSegment%, 1) = ZPosition1
XNoseConePos(ZSegment%, CordSegment%, 1) = -ZPosition1 * TanTheta * COS(2 *
3.14159 * (CordSegment% + .5) / NumNoseConeRadSeg%)
YNoseConePos(ZSegment%, CordSegment%, 1) = ZPosition1 * TanTheta * SIN(2 *
3.14159 * (CordSegment% + .5) / NumNoseConeRadSeg%)
ZNoseConePos(ZSegment%, 2) = ZPosition2
XNoseConePos(ZSegment%, CordSegment%, 2) = -ZPosition2 * TanTheta * COS(2 *
3.14159 * (CordSegment% + .5) / NumNoseConeRadSeg%)
YNoseConePos(ZSegment%, CordSegment%, 2) = ZPosition2 * TanTheta * SIN(2 *
3.14159 * (CordSegment% + .5) / NumNoseConeRadSeg%)
ZNoseConePos(ZSegment%, 3) = ZPosition2
XNoseConePos(ZSegment%, CordSegment%, 3) = -ZPosition2 * TanTheta * COS(2 *
3.14159 * (CordSegment% - .5) / NumNoseConeRadSeg%)
YNoseConePos(ZSegment%, CordSegment%, 3) = ZPosition2 * TanTheta * SIN(2 *
3.14159 * (CordSegment% - .5) / NumNoseConeRadSeg%)
ZNoseConePos(ZSegment%, 4) = ZPosition1
XNoseConePos(ZSegment%, CordSegment%, 4) = -ZPosition1 * TanTheta * COS(2 *
3.14159 * (CordSegment% - .5) / NumNoseConeRadSeg%)
YNoseConePos(ZSegment%, CordSegment%, 4) = ZPosition1 * TanTheta * SIN(2 *

```

```

3.14159 * (CordSegment% - .5) / NumNoseConeRadSeg%)
' the facet areas are calculated
NoseConeArea(ZSegment%) = MaxNoseConeChordLength * ((ZPosition1 + ZPosition2) /
2) * DeltaZNoseCone / (LengthNoseCone * CosTheta)
' the facet normal vector components are
' calculated
ZNoseConeNormal = -SinTheta
XNoseConeNormal(CordSegment%) = -CosTheta * COS(2 * 3.14159 * CordSegment% /
NumNoseConeRadSeg%)
YNoseConeNormal(CordSegment%) = CosTheta * SIN(2 * 3.14159 * CordSegment% /
NumNoseConeRadSeg%)
NEXT CordSegment%
NEXT ZSegment%

```

END SUB

SUB CalcScreenSize

```

*****
THIS SUBROUTINE CALCULATES AN APPROPRIATE SCALE FOR THE GRAPHICS DISPLAY
WINDOW. IT OPERATES BY FIRST TRANSFORMING THE PREVIOUSLY DETERMINED
PROJECTILE EXTREME POSITIONS FROM BODY TO SPACE COORDINATES. CALCULATIONS
ARE THEN PERFORMED TO DETERMINE WHETHER THE GRAPHIC IMAGE SIZE IS
CONSTRAINED
BY THE SIZE OF THE GRAPHIC WINDOW IN THE HORIZONTAL OR VERTICAL DIRECTION.
AN APPROPRIATE SCALE FACTOR IS THEN COMPUTED.
*****

```

```

SHARED XBoxMin, XBoxMax, YBoxMin, YBoxMax, ZBoxMin, ZBoxMax, Scale
SHARED Control$, ZSpaceMin, ZSpaceMax, XSpaceMin, XSpaceMax, YSpaceMin
SHARED YSpaceMax, ScreenWidth, ScreenHeight

```

```

DIM ZM(2), YM(2), XM(2)

```

'projectile extreme position values are
'transferred to array variables to
'facilitate computation.

```

ZM(1) = ZBoxMin
ZM(2) = ZBoxMax
YM(1) = YBoxMin
YM(2) = YBoxMax
XM(1) = XBoxMin
XM(2) = XBoxMax

```

```

ZSpaceMin = 9999
ZSpaceMax = -9999

```

```

YSpaceMin = 9999
YSpaceMax = -9999

```

```

XSpaceMin = 9999
XSpaceMax = -9999

```

'extreme projectile positions in the body
'coordinate system are transformed to
'the viewer, or space, coordinate system.

```

FOR K% = 1 TO 2
  FOR J% = 1 TO 2
    FOR I% = 1 TO 2
      CALL TransCoordBS(XM(I%), YM(J%), ZM(K%), XSpace, YSpace, ZSpace)
      IF (XSpace > XSpaceMax) THEN XSpaceMax = XSpace
      IF (XSpace < XSpaceMin) THEN XSpaceMin = XSpace
      IF (YSpace > YSpaceMax) THEN YSpaceMax = YSpace
      IF (YSpace < YSpaceMin) THEN YSpaceMin = YSpace
      IF (ZSpace > ZSpaceMax) THEN ZSpaceMax = ZSpace
      IF (ZSpace < ZSpaceMin) THEN ZSpaceMin = ZSpace
    
```

```

      NEXT I%
    NEXT J%
  NEXT K%

```

'the ratio of the space frame extreme
'positions in the z and y directions are
'compared to the ratio of the graphic
'screen's dimensions in the horizontal
'and vertical directions to determine the
'more restrictive dimension. a graphic
'scale factor is then calculated.

```

IF (ABS(ZSpaceMax - ZSpaceMin) / ScreenWidth < ABS(YSpaceMax - YSpaceMin) /
    ScreenHeight) THEN
  Scale = ScreenHeight / ABS(YSpaceMax - YSpaceMin)
  Control$ = "Y"
END IF

```

```

IF (ABS(ZSpaceMax - ZSpaceMin) / ScreenWidth >= ABS(YSpaceMax - YSpaceMin) /
    ScreenHeight) THEN
  Scale = ScreenWidth / ABS(ZSpaceMax - ZSpaceMin)
  Control$ = "Z"
END IF

```

```

END SUB

```

```

SUB Eclipse (XTest, YTest, ZTest, CurrentFinNumber%, FinUnitCOSValue, Type$, Ans%)

```

```

*****

```

'THIS SUBROUTINE DETERMINES WHETHER THE VIEW OF A GIVEN FACET WILL BE BLOCKED
'BY ANY OTHER FACET. A NUMBER OF SYMMETRY BASED ASSUMPTIONS ARE USED TO
'SIMPLIFY THIS PROCEDURE.

- ' 1) THE UNIT NORMAL VECTOR OF ALL THE FACETS CHECKED BY THIS ROUTINE MAKE
' AN ANGLE WITH THE UNIT VECTOR TOWARDS THE VIEWER THAT HAS A POSITIVE
' COSINE
- ' 2) NOSE CONE AND BODY FACETS DO NOT REQUIRE THIS TYPE OF TESTING
- ' 3) THE NOSE CONE AND BODY FACETS ARE ALWAYS CLOSER TO THE VIEWER THAN
' THE FIN FACETS
- ' 4) THE NOSE CONE, BODY, AND AFTBODY WILL NEVER BLOCK A FACET ON A FIN FOR
' WHICH THE UNIT VECTOR THAT IS IN THE PLANE OF THE FIN AND PERPENDICULAR
' TO THE LONGITUDINAL BODY AXIS MAKES AN ANGLE WITH THE UNIT VECTOR
' TOWARDS THE VIEWER THAT HAS A POSITIVE COSINE
- ' 5) THE NOSE CONE AND BODY WILL NEVER BLOCK AN AFTBODY FACET
- ' 6) A FACET OF A GIVEN FIN WILL NEVER BE BLOCKED BY ANOTHER FACET IN THAT
' FIN
- ' 7) AN AFTBODY FACET CAN ONLY BE BLOCKED BY A FACET ON A FIN FOR WHICH THE
' DOT PRODUCT BETWEEN THE UNIT VECTOR THAT IS IN THE PLANE OF THE FIN AND
' PERPENDICULAR TO THE LONGITUDINAL BODY AXIS AND THE UNIT VECTOR TOWARD
' THE VIEWER HAS A NON-NEGATIVE VALUE
- ' 8) A FACET ON A FIN CAN ONLY BE BLOCKED BY A FACET ON ANOTHER FIN FOR WHICH
' THE DOT PRODUCT BETWEEN THE UNIT VECTOR THAT IS IN THE PLANE OF THE FIN
' AND PERPENDICULAR TO THE LONGITUDINAL BODY AXIS AND THE UNIT VECTOR
' TOWARDS THE VIEWER HAS A VALUE CLOSER TO ONE.
- ' 9) AN AFTBODY FACET WILL NEVER BE BLOCKED BY ANOTHER AFTBODY FACET
- ' 10) AN AFTBODY FACET WILL NEVER BLOCK A FIN FACET ON A FIN FOR WHICH THE
' DOT PRODUCT BETWEEN THE UNIT VECTOR THAT IS IN THE PLANE OF THE FIN AND
' PERPENDICULAR TO THE LONGITUDINAL BODY AXIS AND THE UNIT VECTOR TOWARD

THE VIEWER HAS A NON-NEGATIVE VALUE

```

*****
SHARED NumNoseConeLongSeg%, NumNoseConeRadSeg%, XNoseConePos()
SHARED YNoseConePos(), ZNoseConePos(), XNoseConeNormal(), YNoseConeNormal()
SHARED ZNoseConeNormal, XBodyNormal(), YBodyNormal(), ZBodyNormal
SHARED NumBodyLongSeg%, NumBodyRadSeg%, NumFinRadSeg%
SHARED XBodyPos(), YBodyPos(), ZBodyPos(), NumFins%
SHARED NumLeadEdgeLongSeg%, NumNonLeadEdgeLongSeg%
SHARED XFinLeadEdgeNormal(), XViewNormal, YFinLeadEdgeNormal()
SHARED YViewNormal, ZFinLeadEdgeNormal, ZViewNormal
SHARED XFinNonLeadEdgeNormal(), YFinNonLeadEdgeNormal()
SHARED ZFinNonLeadEdgeNormal, XFinEdgePos(), YFinEdgePos(), ZFinEdgePos()
SHARED XFinSideNormal(), YFinSideNormal(), ZFinSideNormal
SHARED XFinPos(), YFinPos(), ZFinPos(), NumAftBodyRadSegPerFin%
SHARED XAftBodyPos(), YAftBodyPos(), ZAftBodyPos()
SHARED XAftBodyNormal(), YAftBodyNormal(), ZAftBodyNormal, Scale
                                'as each projectile facet is considered
                                'its position is denoted by a dot. the
                                'following parameters determine the
                                'appearance of this dot

NumBlinks% = 1
BlinkDuration = 1
NewColor = 15

                                'initial state set to nonhidden condition
Ans% = 1
                                'simplification #4 is tested
IF ((FinUnitCOSValue > 0) AND (Type$ = "Fin")) THEN GOTO SkipNoseConeAndBody
                                'simplification #5 is tested

IF (Type$ = "AftBody") THEN GOTO SkipNoseConeAndBody
                                'checking for blocking by nose cone
                                'facets

                                'each nose cone transverse segment is
                                'considered
FOR ZSegment% = 0 TO NumNoseConeLongSeg% - 1
                                'each radial facet within the transverse
                                'segment is considered
    FOR CordSegment% = 0 TO NumNoseConeRadSeg% - 1
                                'only those nose cone facets that have a
                                'normal vector that points "towards" the
                                'viewer are considered
        NormalDotProduct = XNoseConeNormal(CordSegment%) * XViewNormal +
                            YNoseConeNormal(CordSegment%) * YViewNormal +
                            ZNoseConeNormal * ZViewNormal
        IF (NormalDotProduct > 0) THEN
                                'the midpoint position of the nose cone
                                'facet under consideration is calculated

            ZNow = 0
            YNow = 0
            FOR Corner% = 1 TO 4
                CALL TransCoordBS(XNoseConePos(ZSegment%, CordSegment%, Corner%),
                                YNoseConePos(ZSegment%, CordSegment%, Corner%),
                                ZNoseConePos(ZSegment%, CordSegment%, Corner%), XSpace, YSpace, ZSpace)
                ZNow = ZNow + ZSpace / 4
                YNow = YNow + YSpace / 4
            NEXT Corner%

                                'the original color of the midpoint
                                'position pixel is determined and saved
            OldColor = POINT(ZNow * Scale, YNow * Scale)
                                'the midpoint position pixel of the nose
                                'cone facet under consideration is flashed

        FOR I% = 1 TO NumBlinks%

```

```

CALL Plot3DPoint(1, YNow, ZNow, OldColor)
FOR T = 1 TO BlinkDuration: NEXT T
CALL Plot3DPoint(1, YNow, ZNow, NewColor)
FOR T = 1 TO BlinkDuration: NEXT T
NEXT I%

```

'the vertical extremes of the possible
'blocking nose cone facet are determined

```

YFacetMin = 9999
YFacetMax = -9999
FOR Corner% = 1 TO 4
    CALL TransCoordBS(XNoseConePos(ZSegment%, CordSegment%, Corner%),
        YNoseConePos(ZSegment%, CordSegment%, Corner%),
        ZNoseConePos(ZSegment%, Corner%), XSpace, YSpace, ZSpace)
    IF (YSpace > YFacetMax) THEN YFacetMax = YSpace
    IF (YSpace < YFacetMin) THEN YFacetMin = YSpace
NEXT Corner%

```

'the midpoint vertical position of the
'facet that is being tested for blockage
'is compared to the vertical extremes of
'the potentially blocking nose cone facet.
'if the midpoint is contained within the
'range of the nose cone facet's extremes,
'then further testing will be performed
'that considers horizontal overlap. if
'not, then this nose cone facet can not
'be blocking.

```

IF ((YFacetMin < YTest) AND (YFacetMax > YTest)) THEN
    'the horizontal extremes of the possible
    'blocking nose cone facet are determined

```

```

ZFacetMin = 9999
ZFacetMax = -9999
FOR Corner% = 1 TO 4
    CALL TransCoordBS(XNoseConePos(ZSegment%, CordSegment%, Corner%),
        YNoseConePos(ZSegment%, CordSegment%, Corner%),
        ZNoseConePos(ZSegment%, Corner%), XSpace, YSpace, ZSpace)
    IF (ZSpace > ZFacetMax) THEN ZFacetMax = ZSpace
    IF (ZSpace < ZFacetMin) THEN ZFacetMin = ZSpace
NEXT Corner%

```

'the midpoint horizontal position of the
'facet that is being tested for blockage
'is compared to the horizontal extremes of
'the potentially blocking nose cone facet.
'if the midpoint is contained within the
'range of the nose cone facet's extremes,
'then it is concluded that the nose cone
'facet will block the facet being tested.

```

IF ((ZFacetMin < ZTest) AND (ZFacetMax > ZTest)) THEN
    Ans% = 0
    BEEP

```

'the nose cone facet midpoint position
'pixel is returned to its original color

```

CALL Plot3DPoint(1, YNow, ZNow, OldColor)
GOTO Hidden

```

'if this nose cone facet is determined not
'to block the facet under consideration,
'then the nose cone facet's midpoint
'position pixel is simply returned to its
'original color

```

ELSE
    CALL Plot3DPoint(1, YNow, ZNow, OldColor)
END IF

```

'if this nose cone facet is determined not
'to block the facet under consideration,
'then the nose cone facet's midpoint
'position pixel is simply returned to its
'original color

```

ELSE
CALL Plot3DPoint(1, YNow, ZNow, OldColor)
END IF
END IF
NEXT CordSegment%
NEXT ZSegment%

'checking for blocking by body facets
'each body transverse segment is
'considered
FOR ZSegment% = 0 TO NumBodyLongSeg% - 1
'each radial facet within the transverse
'segment is considered
FOR CordSegment% = 0 TO NumBodyRadSeg% - 1
'only those body facets that have a normal
'vector that points "towards" the viewer
'are considered
NormalDotProduct = XBodyNormal(CordSegment%) * XViewNormal +
YBodyNormal(CordSegment%) * YViewNormal +
ZBodyNormal * ZViewNormal
IF (NormalDotProduct > 0) THEN
'the midpoint position of the body facet
'under consideration is calculated

ZNow = 0
YNow = 0
FOR Corner% = 1 TO 4
CALL TransCoordBS(XBodyPos(CordSegment%, Corner%),
YBodyPos(CordSegment%, Corner%), ZBodyPos(ZSegment%,
Corner%), XSpace, YSpace, ZSpace)

ZNow = ZNow + ZSpace / 4
YNow = YNow + YSpace / 4
NEXT Corner%

'the original color of the midpoint
'position pixel is determined and saved
OldColor = POINT(ZNow * Scale, YNow * Scale)
'the midpoint position pixel of the body
'facet under consideration is flashed

FOR I% = 1 TO NumBlinks%
CALL Plot3DPoint(1, YNow, ZNow, OldColor)
FOR T = 1 TO BlinkDuration: NEXT T
CALL Plot3DPoint(1, YNow, ZNow, NewColor)
FOR T = 1 TO BlinkDuration: NEXT T
NEXT I%

'the vertical extremes of the possible
'blocking body facet are determined
YFacetMin = 9999
YFacetMax = -9999
FOR Corner% = 1 TO 4
CALL TransCoordBS(XBodyPos(CordSegment%, Corner%),
YBodyPos(CordSegment%, Corner%), ZBodyPos(ZSegment%,
Corner%), XSpace, YSpace, ZSpace)
IF (YSpace > YFacetMax) THEN YFacetMax = YSpace
IF (YSpace < YFacetMin) THEN YFacetMin = YSpace
NEXT Corner%

'the midpoint vertical position of the
'facet that is being tested for blockage
'is compared to the vertical extremes of
'the potentially blocking body facet. if
'the midpoint is contained within the
'range of the body facet's extremes, then
'further testing will be performed that
'considers horizontal overlap. if
'not, then this body facet can not be
'blocking.
IF ((YFacetMin < YTest) AND (YFacetMax > YTest)) THEN
'the horizontal extremes of the possible

```



```

'blocking body facet are determined
ZFacetMin = 9999
ZFacetMax = -9999
FOR Corner% = 1 TO 4
    CALL TransCoordBS(XBodyPos(CordSegment%, Corner%),
        YBodyPos(CordSegment%, Corner%), ZBodyPos(ZSegment%,
        Corner%), XSpace, YSpace, ZSpace)
    IF (ZSpace > ZFacetMax) THEN ZFacetMax = ZSpace
    IF (ZSpace < ZFacetMin) THEN ZFacetMin = ZSpace
NEXT Corner%

'if this body facet is determined not to
'block the facet under consideration,
'then the body facet's midpoint position
'pixel is simply returned to its original
'color
'if this body facet is determined not to
'block the facet under consideration,
'then the body facet's midpoint position
'pixel is simply returned to its original
'color

IF ((ZFacetMin < ZTest) AND (ZFacetMax > ZTest)) THEN
    Ans% = 0
    BEEP

    'the body facet midpoint position pixel
    'is returned to its original color
    CALL Plot3DPoint(1, YNow, ZNow, OldColor)
    GOTO Hidden

ELSE
    CALL Plot3DPoint(1, YNow, ZNow, OldColor)
END IF

ELSE
    CALL Plot3DPoint(1, YNow, ZNow, OldColor)
END IF
END IF
NEXT CordSegment%
NEXT ZSegment%

SkipNoseConeAndBody:

'checking for blocking by fin facets
'each fin is considered
FOR FinNumber% = 0 TO NumFins% - 1
    'simplification #6 is tested
    IF ((FinNumber% = CurrentFinNumber%) AND (Type$ = "Fin")) THEN GOTO SkipFin
    'the x and y components in the body
    'coordinate system are determined for a
    'unit vector in the fin under
    'consideration that is normal to the
    'longitudinal axis
    TestFinUnitRadXVector = -COS(2 * 3.14159 * FinNumber% / NumFins%)
    TestFinUnitRadYVector = SIN(2 * 3.14159 * FinNumber% / NumFins%)

    'this unit vector is dotted with the unit
    'vector pointing towards the viewer to
    'determine whether the unit vector in the
    'fin points towards or away from the
    'viewer
    TestFinUnitCOSValue = TestFinUnitRadXVector * XViewNormal + TestFinUnitRadYVector *

```

```

YViewNormal
'simplification #7 is tested
IF ((TestFinUnitCOSValue < 0) AND (Type$ = "AftBody")) THEN GOTO SkipFin
'simplification #8 is tested
IF ((TestFinUnitCOSValue < FinUnitCOSValue) AND (Type$ = "Fin")) THEN GOTO SkipFin
'each longitudinal segment of the fin is
'considered
FOR LeadEdgeLongSegNumber% = 0 TO NumLeadEdgeLongSeg% +
    NumNonLeadEdgeLongSeg% - 1
    'each radial segment of the longitudinal
    'segment is considered
    FOR FinRadSegNumber% = 0 TO NumFinRadSeg% - 1
        'both sides of the radial segment are
        'considered
        FOR SideNumber% = 1 TO 2
            'only those fin facets that have a normal
            'vector that points "towards" the viewer
            'are considered
            NormalDotProduct = XFinSideNormal(FinNumber%, SideNumber%) * XViewNormal +
            YFinSideNormal(FinNumber%, SideNumber%) * YViewNormal
            IF (NormalDotProduct > 0) THEN
                'the midpoint position of the fin facet
                'under consideration is calculated

                ZNow = 0
                YNow = 0
                FOR Corner% = 1 TO 4
                    CALL TransCoordBS(XFinPos(FinNumber%, LeadEdgeLongSegNumber%,
                        FinRadSegNumber%, SideNumber%, Corner%),
                        YFinPos(FinNumber%, LeadEdgeLongSegNumber%,
                        FinRadSegNumber%, SideNumber%, Corner%),
                        ZFinPos(LeadEdgeLongSegNumber%, Corner%), XSpace, YSpace,
                        ZSpace)
                    ZNow = ZNow + ZSpace / 4
                    YNow = YNow + YSpace / 4
                NEXT Corner%

                'the original color of the midpoint
                'position pixel is determined and saved
                OldColor = POINT(ZNow * Scale, YNow * Scale)
                'the midpoint position pixel of the fin
                'facet under consideration is flashed

                FOR I% = 1 TO NumBlinks%
                    CALL Plot3DPoint(1, YNow, ZNow, OldColor)
                    FOR T = 1 TO BlinkDuration: NEXT T
                    CALL Plot3DPoint(1, YNow, ZNow, NewColor)
                    FOR T = 1 TO BlinkDuration: NEXT T
                NEXT I%

                'the farthest distance of the fin facet
                'from the viewer is determined

                XFacetMax = -9999
                FOR Corner% = 1 TO 4
                    CALL TransCoordBS(XFinPos(FinNumber%, LeadEdgeLongSegNumber%,
                        FinRadSegNumber%, SideNumber%, Corner%),
                        YFinPos(FinNumber%, LeadEdgeLongSegNumber%,
                        FinRadSegNumber%, SideNumber%, Corner%),
                        ZFinPos(LeadEdgeLongSegNumber%, Corner%), XSpace, YSpace,
                        ZSpace)
                    IF (XSpace > XFacetMax) THEN XFacetMax = XSpace
                NEXT Corner%

                'further testing continues only if the
                'farthest distance of the fin facet from
                'the viewer is less than the distance to
                'the projectile facet under consideration

                IF (XFacetMax < XTest) THEN

                    'the vertical extremes of the possible
                    'blocking fin facet are determined
                    YFacetMin = 9999

```

```

YFacetMax = -9999
FOR Corner% = 1 TO 4
    CALL TransCoordBS(XFinPos(FinNumber%, LeadEdgeLongSegNumber%,
        FinRadSegNumber%, SideNumber%, Corner%),
        YFinPos(FinNumber%, LeadEdgeLongSegNumber%,
        FinRadSegNumber%, SideNumber%, Corner%), ZFinPos(
        LeadEdgeLongSegNumber%, Corner%), XSpace, YSpace,
        ZSpace)
    IF (YSpace > YFacetMax) THEN YFacetMax = YSpace
    IF (YSpace < YFacetMin) THEN YFacetMin = YSpace
NEXT Corner%

'the midpoint vertical position of the
'facet that is being tested for blockage
'is compared to the vertical extremes of
'the potentially blocking fin facet. if
'the midpoint is contained within the
'range of the fin facet's extremes, then
'further testing will be performed that
'considers horizontal overlap. if
'not, then this fin facet can not be
'blocking.
IF ((YFacetMin < YTest) AND (YFacetMax > YTest)) THEN
    'the horizontal extremes of the possible
    'blocking fin facet are determined

    ZFacetMin = 9999
    ZFacetMax = -9999
    FOR Corner% = 1 TO 4
        CALL TransCoordBS(XFinPos(FinNumber%, LeadEdgeLongSegNumber%,
            FinRadSegNumber%, SideNumber%, Corner%),
            YFinPos(FinNumber%, LeadEdgeLongSegNumber%,
            FinRadSegNumber%, SideNumber%, Corner%), ZFinPos(
            LeadEdgeLongSegNumber%, Corner%), XSpace, YSpace,
            ZSpace)
        IF (ZSpace > ZFacetMax) THEN ZFacetMax = ZSpace
        IF (ZSpace < ZFacetMin) THEN ZFacetMin = ZSpace
    NEXT Corner%

    'the midpoint horizontal position of the
    'facet that is being tested for blockage
    'is compared to the horizontal extremes of
    'the potentially blocking fin facet. if
    'the midpoint is contained within the
    'range of the fin facet's extremes, then
    'it is concluded that the fin facet will
    'block the facet being tested.
    IF ((ZFacetMin < ZTest) AND (ZFacetMax > ZTest)) THEN
        BEEP
        'the fin facet midpoint position pixel
        'is returned to its original color
        CALL Plot3DPoint(1, YNow, ZNow, OldColor)
        Ans% = 0
        GOTO Hidden

        'if this fin facet is determined not to
        'block the facet under consideration,
        'then the fin facet's midpoint position
        'pixel is simply returned to its original
        'color
    ELSE
        CALL Plot3DPoint(1, YNow, ZNow, OldColor)
    END IF

    'if this fin facet is determined not to
    'block the facet under consideration,
    'then the fin facet's midpoint position
    'pixel is simply returned to its original
    'color
ELSE
    CALL Plot3DPoint(1, YNow, ZNow, OldColor)

```

```

END IF

'if this fin facet is determined not to
'block the facet under consideration,
'then the fin facet's midpoint position
'pixel is simply returned to its original
'color

ELSE
CALL Plot3DPoint(1, YNow, ZNow, OldColor)
END IF
END IF
NEXT SideNumber%
NEXT FinRadSegNumber%

'the leading edge of each longitudinal
'segment of the fin is considered
IF (LeadEdgeLongSegNumber% < NumLeadEdgeLongSeg%) THEN
NormalDotProduct = XFinLeadEdgeNormal(FinNumber%) * XViewNormal +
YFinLeadEdgeNormal(FinNumber%) * YViewNormal +
ZFinLeadEdgeNormal * ZViewNormal

ELSE
NormalDotProduct = XFinNonLeadEdgeNormal(FinNumber%) * XViewNormal +
YFinNonLeadEdgeNormal(FinNumber%) * YViewNormal
END IF

'only those fin facets that have a normal
'vector that points "towards" the viewer
'are considered
IF (NormalDotProduct > 0) THEN

'the midpoint position of the fin facet
'under consideration is calculated
ZNow = 0
YNow = 0
FOR Corner% = 1 TO 4
CALL TransCoordBS(XFinEdgePos(FinNumber%, LeadEdgeLongSegNumber%,
Corner%), YFinEdgePos(FinNumber%,
LeadEdgeLongSegNumber%, Corner%),
ZFinEdgePos(LeadEdgeLongSegNumber%, Corner%), XSpace,
YSpace, ZSpace)

ZNow = ZNow + ZSpace / 4
YNow = YNow + YSpace / 4
NEXT Corner%

'the original color of the midpoint
'position pixel is determined and saved
OldColor = POINT(ZNow * Scale, YNow * Scale)

'the midpoint position pixel of the fin
'facet under consideration is flashed
FOR I% = 1 TO NumBlinks%
CALL Plot3DPoint(1, YNow, ZNow, OldColor)
FOR T = 1 TO BlinkDuration: NEXT T
CALL Plot3DPoint(1, YNow, ZNow, NewColor)
FOR T = 1 TO BlinkDuration: NEXT T
NEXT I%

'the farthest distance of the fin facet
'from the viewer is determined
XFacetMax = -9999
FOR Corner% = 1 TO 4
CALL TransCoordBS(XFinEdgePos(FinNumber%, LeadEdgeLongSegNumber%,
Corner%), YFinEdgePos(FinNumber%,
LeadEdgeLongSegNumber%, Corner%),
ZFinEdgePos(LeadEdgeLongSegNumber%, Corner%), XSpace,
YSpace, ZSpace)
IF (XSpace > XFacetMax) THEN XFacetMax = XSpace
NEXT Corner%

'further testing continues only if the
'farthest distance of the fin facet from
'the viewer is less than the distance to
'the projectile facet under consideration
IF (XFacetMax < XTest) THEN

```

```

                                'the vertical extremes of the possible
                                'blocking fin facet are determined
YFacetMin = 9999
YFacetMax = -9999
FOR Corner% = 1 TO 4
    CALL TransCoordBS(XFinEdgePos(FinNumber%, LeadEdgeLongSegNumber%,
                                Corner%), YFinEdgePos(FinNumber%,
                                LeadEdgeLongSegNumber%, Corner%),
                                ZFinEdgePos(LeadEdgeLongSegNumber%, Corner%), XSpace,
                                YSpace, ZSpace)
    IF (YSpace > YFacetMax) THEN YFacetMax = YSpace
    IF (YSpace < YFacetMin) THEN YFacetMin = YSpace
NEXT Corner%

                                'the midpoint vertical position of the
                                'facet that is being tested for blockage
                                'is compared to the vertical extremes of
                                'the potentially blocking fin facet. if
                                'the midpoint is contained within the
                                'range of the fin facet's extremes, then
                                'further testing will be performed that
                                'considers horizontal overlap. if
                                'not, then this fin facet can not be
                                'blocking.
IF ((YFacetMin < YTest) AND (YFacetMax > YTest)) THEN
                                'the horizontal extremes of the possible
                                'blocking fin facet are determined
ZFacetMin = 9999
ZFacetMax = -9999
FOR Corner% = 1 TO 4
    CALL TransCoordBS(XFinEdgePos(FinNumber%, LeadEdgeLongSegNumber%,
                                Corner%), YFinEdgePos(FinNumber%,
                                LeadEdgeLongSegNumber%, Corner%),
                                ZFinEdgePos(LeadEdgeLongSegNumber%, Corner%), XSpace,
                                YSpace, ZSpace)
    IF (ZSpace > ZFacetMax) THEN ZFacetMax = ZSpace
    IF (ZSpace < ZFacetMin) THEN ZFacetMin = ZSpace
NEXT Corner%

                                'the midpoint horizontal position of the
                                'facet that is being tested for blockage
                                'is compared to the horizontal extremes of
                                'the potentially blocking fin facet. if
                                'the midpoint is contained within the
                                'range of the fin facet's extremes, then
                                'it is concluded that the fin facet will
                                'block the facet being tested.
IF ((ZFacetMin < ZTest) AND (ZFacetMax > ZTest)) THEN
    BEEP
                                'the fin facet midpoint position pixel
                                'is returned to its original color
    CALL Plot3DPoint(1, YNow, ZNow, OldColor)
    Ans% = 0
    GOTO Hidden

                                'if this fin facet is determined not to
                                'block the facet under consideration,
                                'then the fin facet's midpoint position
                                'pixel is simply returned to its original
                                'color
ELSE
    CALL Plot3DPoint(1, YNow, ZNow, OldColor)
END IF

                                'if this fin facet is determined not to
                                'block the facet under consideration,
                                'then the fin facet's midpoint position
                                'pixel is simply returned to its original
                                'color
ELSE

```

```

CALL Plot3DPoint(1, YNow, ZNow, OldColor)
END IF

'if this fin facet is determined not to
'block the facet under consideration,
'then the fin facet's midpoint position
'pixel is simply returned to its original
'color

ELSE
CALL Plot3DPoint(1, YNow, ZNow, OldColor)
END IF
END IF
NEXT LeadEdgeLongSegNumber%

SkipFin:
NEXT FinNumber%

'checking for blocking by aftbody facets
'checking for simplification #9

IF (Type$ = "AftBody") THEN GOTO SkipAftBody

'checking for simplification #10
IF ((FinUnitCOSValue > 0) AND (Type$ = "Fin")) THEN GOTO SkipAftBody
'each transverse slice of the aftbody
'is considered
FOR ZSegment% = 0 TO NumLeadEdgeLongSeg% + NumNonLeadEdgeLongSeg% - 1
'each aftbody area between adjacent fins
'is considered

FOR FinNumber% = 0 TO NumFins% - 1

'the radial facets in each aftbody area
'are considered
FOR AftBodyRadSegNumber% = 0 TO NumAftBodyRadSegPerFin% - 1
NormalDotProduct = XAftBodyNormal(FinNumber%, AftBodyRadSegNumber%) *
XViewNormal + YAftBodyNormal(FinNumber%,
AftBodyRadSegNumber%) * YViewNormal
'only those aftbody facets with normals
'that point "toward" the viewer are
'considered

IF (NormalDotProduct > 0) THEN

'the midpoint position of the aftbody
'facet is determined

ZNow = 0
YNow = 0
FOR Corner% = 1 TO 4
CALL TransCoordBS(XAftBodyPos(FinNumber%, AftBodyRadSegNumber%,
Corner%), YAftBodyPos(FinNumber%,
AftBodyRadSegNumber%, Corner%),
ZAftBodyPos(ZSegment%, Corner%), XSpace, YSpace,
ZSpace)
ZNow = ZNow + ZSpace / 4
YNow = YNow + YSpace / 4
NEXT Corner%

'the original color of the midpoint
'position pixel is determined and saved
OldColor = POINT(ZNow * Scale, YNow * Scale)
'the midpoint position pixel of the
'aftbody facet is flashed

FOR I% = 1 TO NumBlinks%
CALL Plot3DPoint(1, YNow, ZNow, OldColor)
FOR T = 1 TO BlinkDuration: NEXT T
CALL Plot3DPoint(1, YNow, ZNow, NewColor)
FOR T = 1 TO BlinkDuration: NEXT T
NEXT I%

'the farthest distance of the aftbody
'facet from the viewer is determined

XFacetMax = -9999
FOR Corner% = 1 TO 4
CALL TransCoordBS(XAftBodyPos(FinNumber%, AftBodyRadSegNumber%,
Corner%), YAftBodyPos(FinNumber%,
AftBodyRadSegNumber%, Corner%),

```

```

                                ZAftBodyPos(ZSegment%, Corner%), XSpace, YSpace,
                                ZSpace)
IF (XSpace > XFacetMax) THEN XFacetMax = XSpace
NEXT Corner%

                                'further testing continues only if the
                                'farthest distance of the aftbody facet
                                'from the viewer is less than the distance
                                'to the projectile facet under consideration

IF (XFacetMax < XTest) THEN

                                'the vertical extremes of the possible
                                'blocking aftbody facet are determined

YFacetMin = 9999
YFacetMax = -9999
FOR Corner% = 1 TO 4
    CALL TransCoordBS(XAftBodyPos(FinNumber%, AftBodyRadSegNumber%,
                                Corner%), YAftBodyPos(FinNumber%,
                                AftBodyRadSegNumber%, Corner%),
                                ZAftBodyPos(ZSegment%, Corner%), XSpace, YSpace,
                                ZSpace)
    IF (YSpace > YFacetMax) THEN YFacetMax = YSpace
    IF (YSpace < YFacetMin) THEN YFacetMin = YSpace
NEXT Corner%

                                'the midpoint vertical position of the
                                'facet that is being tested for blockage
                                'is compared to the vertical extremes of
                                'the potentially blocking aftbody facet.
                                'if the midpoint is contained within the
                                'range of the aftbody facet's extremes,
                                'then further testing will be performed
                                'that considers horizontal overlap. if
                                'not, then this aftbody facet can not be
                                'blocking.

IF ((YFacetMin < YTest) AND (YFacetMax > YTest)) THEN
                                'the horizontal extremes of the possible
                                'blocking aftbody facet are determined

ZFacetMin = 9999
ZFacetMax = -9999
FOR Corner% = 1 TO 4
    CALL TransCoordBS(XAftBodyPos(FinNumber%, AftBodyRadSegNumber%,
                                Corner%), YAftBodyPos(FinNumber%,
                                AftBodyRadSegNumber%, Corner%),
                                ZAftBodyPos(ZSegment%, Corner%), XSpace, YSpace,
                                ZSpace)
    IF (ZSpace > ZFacetMax) THEN ZFacetMax = ZSpace
    IF (ZSpace < ZFacetMin) THEN ZFacetMin = ZSpace
NEXT Corner%

                                'the midpoint horizontal position of the
                                'facet that is being tested for blockage
                                'is compared to the horizontal extremes of
                                'the potentially blocking aftbody facet.
                                'if the midpoint is contained within the
                                'range of the aftbody facet's extremes,
                                'then it is concluded that the aftbody
                                'facet will block the facet being tested.

IF ((ZFacetMin < ZTest) AND (ZFacetMax > ZTest)) THEN
    BEEP

                                'the aftbody facet midpoint position pixel
                                'is returned to its original color

    CALL Plot3DPoint(1, YNow, ZNow, OldColor)
    Ans% = 0
    GOTO Hidden

                                'if this aftbody facet is determined not
                                'to block the facet under consideration,
                                'then the aftbody facet's midpoint
                                'position pixel is simply returned to its
                                'original color

```

```

ELSE
CALL Plot3DPoint(1, YNow, ZNow, OldColor)
END IF
'if this aftbody facet is determined not
'to block the facet under consideration,
'then the aftbody facet's midpoint
'position pixel is simply returned to its
'original color

ELSE
CALL Plot3DPoint(1, YNow, ZNow, OldColor)
END IF
'if this aftbody facet is determined not
'to block the facet under consideration,
'then the aftbody facet's midpoint
'position pixel is simply returned to its
'original color

ELSE
CALL Plot3DPoint(1, YNow, ZNow, OldColor)
END IF
END IF
NEXT AftBodyRadSegNumber%
NEXT FinNumber%
NEXT ZSegment%

```

SkipAftBody:

Hidden:

END SUB

SUB Init3DDisplay

'THIS SUBROUTINE INITIALIZES THE GRAPHIC VIEWPORT USING THE PREVIOUSLY
'DETERMINED SCALE FACTOR. THE GRAPHIC DISPLAY PARAMETERS ARE THEN OUTPUT
'IN LEADER FORMAT TO THE DATA STORAGE FILE. FINALLY, THE GRAPHIC DISPLAY
'COLORS ARE DEFINED.

SHARED YSpaceMin, YSpaceMax, ZSpaceMin, ZSpaceMax, Scale, Control\$
SHARED ScreenWidth, ScreenHeight, AspectRatio

DIM C&(15)

'the graphic viewport is initializes to
'cover the entire monitor screen

SCREEN 12

VIEW (1, 1)-(ScreenWidth, ScreenHeight), 1

'the viewport coordinate system is
'defined. the overlap variables pertain to
'those portions of the less restrictive
'direction that are essentially left empty

IF (Control\$ = "Y") THEN

ZOverlap = ScreenWidth - Scale * ABS(ZSpaceMax - ZSpaceMin)

WindowX1 = ZSpaceMin * Scale - ZOverlap / 2

WindowY1 = YSpaceMin * Scale

WindowX2 = ZSpaceMax * Scale + ZOverlap / 2

WindowY2 = YSpaceMax * Scale

WINDOW ((WindowX1 + WindowX2) / 2 - AspectRatio * (WindowX2 - WindowX1) / 2,
WindowY1)-((WindowX1 + WindowX2) / 2 + AspectRatio *
(WindowX2 - WindowX1) / 2, WindowY2)

END IF

IF (Control\$ = "Z") THEN

YOverlap = ScreenHeight - Scale * ABS(YSpaceMax - YSpaceMin)


```

WindowX1 = ZSpaceMin * Scale
WindowY1 = YSpaceMin * Scale - YOverlap / 2
WindowX2 = ZSpaceMax * Scale
WindowY2 = YSpaceMax * Scale + YOverlap / 2
WINDOW ((WindowX1 + WindowX2) / 2 - AspectRatio * (WindowX2 - WindowX1) / 2,
        WindowY1) - ((WindowX1 + WindowX2) / 2 + AspectRatio *
        (WindowX2 - WindowX1) / 2, WindowY2)

END IF

PRINT #1, "graphic scale factor: "
PRINT #1, Scale
PRINT #1, "WindowX1: "
PRINT #1, WindowX1
PRINT #1, "WindowY1: "
PRINT #1, WindowY1
PRINT #1, "WindowX2: "
PRINT #1, WindowX2
PRINT #1, WindowY2

Blue = 63
Breen = 63
Red = 63

FOR I% = 3 TO 15
    C&(I%) = 65536 * INT(((I% - 3) / 12) * Blue) + 256 * INT(((I% - 3) / 12) * Green) +
    INT(((I% - 3) / 12) * Red)
NEXT I%

C&(0) = 0
C&(1) = 32
C&(2) = 26
PALETTE USING C&(0)

END SUB

SUB InputParameters
*****
THIS SUBROUTINE REQUESTS THE USER TO INPUT PARAMETER VALUES FOR THE
PROJECTILE'S DIMENSIONS, TEMPERATURE, MATERIAL CHARACTERISTICS, AND
ORIENTATION. THIS INFORMATION IS THEN SAVED AS LEADER INFORMATION IN
A DATA FILE USING A FILE NAME WHICH IS SUPPLIED BY THE USER.
*****

SHARED LengthNoseCone, DeltaZNoseCone, NumNoseConeLongSeg%, RadNoseCone
SHARED NumNoseConeRadSeg%, LengthBody, DeltaZBody, NumBodyLongSeg%
SHARED RadBody, NumBodyRadSeg%, NumFins%, ThickFin, LengthBaseFin
SHARED LengthLeadEdgeFin, DeltaZFin, NumLeadEdgeLongSeg%
SHARED NumNonLeadEdgeLongSeg%, HeightFin, DeltaRadFin, NumFinRadSeg%
SHARED NumAftBodyRadSegPerFin%, Euler(), File1$, NoseForwTemp
SHARED NoseRearTemp, NoseEmis, BodyForwTemp, BodyRearTemp, BodyEmis
SHARED FinOuterWRTInnerTemp, FinLeadTemp, FinTrailTemp, FinEmis
SHARED AftBodyForwTemp, AftBodyRearTemp, AftBodyEmis

CLS

INPUT "Enter the length of the nose cone in millimeters: "; LengthNoseCone

```

'graphic screen definition parameters are
'saved in the data storage file

'palette colors 3 through 15 are defined
'to be shades of gray with 3 being black
'and 15 being white.

'palette color 0 is defined to be black
'for "erasing" purposes, color 1 will
'serve as the background color, and color
'2 will be used for drawing construction
'lines

'the user is requested to enter projectile
'parameter information

```

LengthNoseCone = LengthNoseCone / 1000
PRINT

INPUT "Enter the nose cone longitudinal segment length in millimeters: "; DeltaZNoseCone
DeltaZNoseCone = DeltaZNoseCone / 1000
PRINT

NumNoseConeLongSeg% = CINT(LengthNoseCone / DeltaZNoseCone)

INPUT "Enter the radius of the nose cone base in millimeters: "; RadNoseCone
RadNoseCone = RadNoseCone / 1000
PRINT

INPUT "Enter the number of nose cone cord segments: "; NumNoseConeRadSeg%
PRINT

INPUT "Enter the length of the body in millimeters: "; LengthBody
LengthBody = LengthBody / 1000
PRINT

INPUT "Enter the body longitudinal segment length in millimeters: "; DeltaZBody
DeltaZBody = DeltaZBody / 1000
PRINT

NumBodyLongSeg% = CINT(LengthBody / DeltaZBody)

INPUT "Enter the radius of the body in millimeters: "; RadBody
RadBody = RadBody / 1000
PRINT

INPUT "Enter the number of body cord segments: "; NumBodyRadSeg%
PRINT

INPUT "Enter the number of fins: "; NumFins%
PRINT

INPUT "Enter the fin thickness in millimeters: "; ThickFin
ThickFin = ThickFin / 1000
PRINT

INPUT "Enter the base length of the fin in millimeters: "; LengthBaseFin
LengthBaseFin = LengthBaseFin / 1000
PRINT

INPUT "Enter the base length of the fin leading edge in millimeters: "; LengthLeadEdgeFin
LengthLeadEdgeFin = LengthLeadEdgeFin / 1000
PRINT

INPUT "Enter the fin longitudinal segment length in millimeters: "; DeltaZFin
DeltaZFin = DeltaZFin / 1000
PRINT

NumLeadEdgeLongSeg% = CINT(LengthLeadEdgeFin / DeltaZFin)
NumNonLeadEdgeLongSeg% = CINT((LengthBaseFin - LengthLeadEdgeFin) / DeltaZFin)

INPUT "Enter the fin height in millimeters: "; HeightFin
HeightFin = HeightFin / 1000
PRINT

INPUT "Enter the fin transverse segment length in millimeters: "; DeltaRadFin
DeltaRadFin = DeltaRadFin / 1000
PRINT

NumFinRadSeg% = CINT(HeightFin / DeltaRadFin)

INPUT "Enter the number of aft body cord segments between fins: ";

```

```

                                NumAftBodyRadSegPerFin%
PRINT
INPUT "Enter the three Euler angles in degrees: "; Euler(1), Euler(2), Euler(3)
FOR I% = 1 TO 3
    Euler(I%) = Euler(I%) * 3.14159 / 180
NEXT I%
PRINT
INPUT "Enter the nose cone forward tip temperature: "; NoseForwTemp
PRINT
INPUT "Enter the nose cone rear base temperature: "; NoseRearTemp
PRINT
INPUT "Enter the nose cone emissivity: "; NoseEmis
PRINT
INPUT "Enter the body forward temperature: "; BodyForwTemp
PRINT
INPUT "Enter the body rear temperature: "; BodyRearTemp
PRINT
INPUT "Enter the body emissivity: "; BodyEmis
PRINT
PRINT "Enter the fin outer edge temperature relative to"
INPUT " the inner edge temperature: "; FinOuterWRTInnerTemp
PRINT
PRINT "Enter the fin leading edge temperature"
INPUT " at the inner edge: "; FinLeadTemp
PRINT
PRINT "Enter the fin trailing edge temperature "
INPUT " at the inner edge: "; FinTrailTemp
PRINT
INPUT "Enter the fin emissivity: "; FinEmis
PRINT
INPUT "Enter the aftbody forward temperature: "; AftBodyForwTemp
PRINT
INPUT "Enter the aftbody rear temperature: "; AftBodyRearTemp
PRINT
INPUT "Enter the aftbody emissivity: "; AftBodyEmis
PRINT
INPUT "Enter the storage data file name: "; File1$
PRINT
                                'the projectile parameters are saved as
                                'leader information in a data file
OPEN "C:\QB45\IRMODEL\" + File1$ FOR OUTPUT AS #1
PRINT #1, "length of nose cone in meters: "
PRINT #1, LengthNoseCone
PRINT #1, "nose cone longitudinal segment length in meters: "
PRINT #1, DeltaZNoseCone
PRINT #1, "number of nose cone longitudinal segments: "
PRINT #1, NumNoseConeLongSeg%
PRINT #1, "nose cone radius in meters: "
PRINT #1, RadNoseCone
PRINT #1, "number of nose cone cord segments: "

```

```

PRINT #1, NumNoseConeRadSeg%
PRINT #1, "length of body in meters: "
PRINT #1, LengthBody
PRINT #1, "body longitudinal segment length in meters: "
PRINT #1, DeltaZBody
PRINT #1, "number of longitudinal body segments: "
PRINT #1, NumBodyLongSeg%
PRINT #1, "body radius in meters: "
PRINT #1, RadBody
PRINT #1, "number of body cord segments: "
PRINT #1, NumBodyRadSeg%
PRINT #1, "number of fins: "
PRINT #1, NumFins%
PRINT #1, "fin thickness in meters: "
PRINT #1, ThickFin
PRINT #1, "total fin base length in meters: "
PRINT #1, LengthBaseFin
PRINT #1, "base length of fin leading edge in meters: "
PRINT #1, LengthLeadEdgeFin
PRINT #1, "fin longitudinal segment length in meters: "
PRINT #1, DeltaZFin
PRINT #1, "number of fin leading edge longitudinal segments: "
PRINT #1, NumLeadEdgeLongSeg%
PRINT #1, "number of fin nonleading edge longitudinal segments: "
PRINT #1, NumNonLeadEdgeLongSeg%
PRINT #1, "fin height in meters: "
PRINT #1, HeightFin
PRINT #1, "fin transverse segment length in meters: "
PRINT #1, DeltaRadFin
PRINT #1, "number of fin radial segments: "
PRINT #1, NumFinRadSeg%
PRINT #1, "number of aft body cord segments between fins: "
PRINT #1, NumAftBodyRadSegPerFin%
PRINT #1, "Euler angle 1: "
PRINT #1, Euler(1) * 180 / 3.14159
PRINT #1, "Euler angle 2: "
PRINT #1, Euler(2) * 180 / 3.14159
PRINT #1, "Euler angle 3: "
PRINT #1, Euler(3) * 180 / 3.14159
PRINT #1, "nose cone forward tip temperature: "
PRINT #1, NoseForwTemp
PRINT #1, "nose cone rear base temperature: "
PRINT #1, NoseRearTemp
PRINT #1, "nose cone emissivity: "
PRINT #1, NoseEmis
PRINT #1, "body forward temperature: "
PRINT #1, BodyForwTemp
PRINT #1, "body rear temperature: "
PRINT #1, BodyRearTemp
PRINT #1, "body emissivity: "
PRINT #1, BodyEmis
PRINT #1, "fin outer edge temperature wrt inner edge temperature: "
PRINT #1, FinOuterWRTInnerTemp
PRINT #1, "fin leading edge temperature at the inner edge: "
PRINT #1, FinLeadTemp
PRINT #1, "fin trailing edge temperature at the inner edge: "
PRINT #1, FinTrailTemp
PRINT #1, "fin emissivity: "
PRINT #1, FinEmis
PRINT #1, "aftbody forward temperature: "
PRINT #1, AftBodyForwTemp
PRINT #1, "aftbody rear temperature: "
PRINT #1, AftBodyRearTemp
PRINT #1, "aftbody emissivity: "
PRINT #1, AftBodyEmis
PRINT #1, "name of this data file: "

```

```

PRINT #1, File1$

END SUB

SUB LoadDataFile (Type$, X(), Y(), Z(), NormalDotProduct, Area, Temp, Emis)
*****

THIS SUBROUTINE IS USED TO LOAD THE INFORMATION ABOUT A FACET INTO THE DATA
STORAGE FILE
*****

PRINT #1, USING "\ \", +#.#### +#.#### +#.#### +#.#### +#.#### +#.#### +#.####
          +#.#### +#.#### +#.#### +#.#### +#.#### +#.#### +#.#### +#.####
          #.##"; Type$, X(1); Y(1); Z(1); X(2); Y(2); Z(2); X(3); Y(3); Z(3); X(4); Y(4);
          Z(4); NormalDotProduct; Area; Temp; Emis

END SUB

SUB Plot3DLine (X, Y, Z, C1)
*****

THIS SUBROUTINE IS USED TO PLOT A LINE FROM THE PREVIOUS GRAPHIC SCREEN
POSITION TO THE NEWLY PROVIDED COORDINATES
*****

    SHARED Scale
    LINE -(Z * Scale, Y * Scale), C1

END SUB

SUB Plot3DPoint (X, Y, Z, C1)
*****

THIS SUBROUTINE IS USED TO PLOT A POINT ON THE GRAPHIC DISPLAY
*****

    SHARED Scale
    PSET (Z * Scale, Y * Scale), C1

END SUB

SUB TransCoordBS (XOld, YOld, ZOld, XSpace, YSpace, ZSpace)
*****

THIS SUBROUTINE TRANSFORMS FROM PROJECTILE BODY COORDINATES TO SPACE
COORDINATES.
*****

    SHARED E()
    DIM COld(3), CNew(3)

    COld(1) = XOld
    COld(2) = YOld
    COld(3) = ZOld

```

```

FOR I% = 1 TO 3
  CNew(I%) = 0
  FOR J% = 1 TO 3
    CNew(I%) = CNew(I%) + COld(J%) * E(I%, J%)
  NEXT J%
NEXT I%

XSpace = CNew(1)
YSpace = CNew(2)
ZSpace = CNew(3)

END SUB

SUB TransCoordSB (XSpace, YSpace, ZSpace, XBody, YBody, ZBody)
*****

THIS SUBROUTINE TRANSFORMS FROM SPACE COORDINATES TO PROJECTILE BODY
COORDINATES.
*****

  SHARED E()

  DIM COld(3), CNew(3)

  COld(1) = XSpace
  COld(2) = YSpace
  COld(3) = ZSpace

  FOR I% = 1 TO 3
    CNew(I%) = 0
    FOR J% = 1 TO 3
      CNew(I%) = CNew(I%) + COld(J%) * E(J%, I%)
    NEXT J%
  NEXT I%

  XBody = CNew(1)
  YBody = CNew(2)
  ZBody = CNew(3)

END SUB

```

APPENDIX B:
PENETRATOR IR EMISSION CALCULATION SOFTWARE

INTENTIONALLY LEFT BLANK.

This software calculates the spectral and spatial distributions of infrared (IR) radiation emitted by a kinetic energy (KE) penetrator. A data file must be input to this program that has been generated by the previously discussed and listed facet model generation software. MicroSoft QuickBasic 4.5 is used as the programming environment. If you have any questions about this code, please contact Tom Kottke at:

AMSRL-WT-WD
Survivability Concepts Branch
Weapons Concepts Division, Bldg. 120
Weapons Technology Directorate
U.S. Army Research Laboratory
Aberdeen Proving Ground, MD 21005-5066
(410) 278-2557

```

                                'subroutines are declared
DECLARE SUB ReadInputData1 ()
DECLARE SUB ReadInputData2 {}
DECLARE SUB DeterPlotColor (Temp, C)
DECLARE SUB Init3DDisp ()
DECLARE SUB Plot3DPoint (X, Y, Z, C1)
DECLARE SUB Plot3DLine (X, Y, Z, C1)
DECLARE SUB DeterPFacet (FacNumber%, SpecWinNumber%, PofL)
DECLARE SUB OutputData ()

CLS
                                'Euler angle variable is dimensioned
DIM Euler(3)
                                'leader data is input from datafile
                                'output file name is specified

CALL ReadInputData1

PRINT "Enter the file name that the calculated spectral data is to be"
INPUT " saved in: "; File2$
                                'other array variables are dimensioned
DIM Type$(NumFacets%), X(NumFacets%, 4), Y(NumFacets%, 4), Z(NumFacets%, 4)
DIM NormalCos(NumFacets%), Area(NumFacets%), Temp(NumFacets%)
DIM Emis(NumFacets%), ZAve(NumFacets%)
                                'facet data is input from datafile

CALL ReadInputData2
                                'minimum and maximum facet temperatures
                                'are determined

TempMin = 9999
TempMax = -9999
FOR I% = 1 TO NumFacets%
    IF (Temp(I%) < TempMin) THEN TempMin = Temp(I%)
    IF (Temp(I%) > TempMax) THEN TempMax = Temp(I%)
NEXT I%
                                'the average horizontal position is
                                'calculated for each facet

FOR I% = 1 TO NumFacets%
    ZAve(I%) = 0
    FOR J% = 1 TO 4
        ZAve(I%) = ZAve(I%) + Z(I%, J%) / 4
    NEXT J%
NEXT I%
                                'the minimum and maximum average

```

```

'horizontal facet positions are
'determined

ZAveMin = 1E+10
ZAveMax = -1E-10

FOR I% = 1 TO NumFacets%
  IF (ZAve(I%) < ZAveMin) THEN ZAveMin = ZAve(I%)
  IF (ZAve(I%) > ZAveMax) THEN ZAveMax = ZAve(I%)
NEXT I%

'the minimum and maximum average
'horizontal facet positions are output to
'the screen to allow the user to determine
'the horizontal range over which IR
'spectral calculations are to be
'performed

PRINT "Minimum Z Average Value: "; ZAveMin
PRINT
PRINT "Maximum Z Average Value: "; ZAveMax
PRINT

'the user enters information regarding the
'spatial and spectral extents over which
'the IR calculations are to be performed

INPUT "Enter the number of spatially resolved regions: "; NumZRegions%
PRINT
PRINT "Enter the minimum and maximum Z values of the"
INPUT " total spatial region: "; ZSPatMin, ZSPatMax
ZSPatSize = (ZSPatMax - ZSPatMin) / NumZRegions%
PRINT
INPUT "Enter the minimum spectral wavelength in microns: "; SpecMin
PRINT
INPUT "Enter the maximum spectral wavelength in microns: "; SpecMax
PRINT
INPUT "Enter the span of each spectral window in microns: "; SpecWindowSize
NumSpecWindows% = (SpecMax - SpecMin) / SpecWindowSize
PRINT

'user enters projectile's range from the
'assumed IR detector. This information is
'used to calculate the intensity of the
'IR radiation that is incident on the
'detector

INPUT "Enter the range to the projectile in meters: "; ProjRange
PRINT

'radiant flux array variables are
'dimensioned
DIM P(NumZRegions%, NumSpecWindows%), PRegion(NumZRegions%)
'3D graphic display is initialized
CALL Init3DDisp

'wire mesh model of penetrator is
'presented graphically in a neutral
'color to illustrate what portions of
'the penetrator are contained in each
'spatial zone

FOR I% = 1 TO NumFacets%
  CALL Plot3DPoint(X(I%, 4), Y(I%, 4), Z(I%, 4), 15)
  FOR J% = 1 TO 4
    CALL Plot3DLine(X(I%, J%), Y(I%, J%), Z(I%, J%), 15)
  NEXT J%
NEXT I%

'the radiant flux from each spatial
'region is calculated

FOR ZRegNumber% = 1 TO NumZRegions%

'the limits of the spatial region under
'consideration are calculated

ZRegMin = ZSPatMin + (ZRegNumber% - 1) * ZSPatSize
ZRegMax = ZSPatMin + ZRegNumber% * ZSPatSize
FOR FacNumber% = 1 TO NumFacets%

```

```

                                'each facet is checked to determine if it
                                'is located in the spatial region under
                                'consideration
IF ((ZAve(FacNumber%) >= ZRegMin) AND (ZAve(FacNumber%) < ZRegMax)) THEN
                                'if a given facet is determined to be
                                'located in the spatial region under
                                'consideration its facet is redrawn in a
                                'color that is indicative of its
                                'temperature
CALL DeterPlotColor(Temp(FacNumber%), C)
CALL Plot3DPoint(X(FacNumber%, 4), Y(FacNumber%, 4), Z(FacNumber%, 4), C)
FOR Corner% = 1 TO 4
    CALL Plot3DLine(X(FacNumber%, Corner%), Y(FacNumber%, Corner%),
                    Z(FacNumber%, Corner%), C)
NEXT Corner%

                                'the contribution of the facet to the
                                'radiance within each spectral zone is
                                'calculated and added to the total
                                'radiance produced by the spatial region
                                'under consideration
FOR SpecWinNumber% = 1 TO NumSpecWindows%
    CALL DeterPFacet(FacNumber%, SpecWinNumber%, PofL)
    P(ZRegNumber%, SpecWinNumber%) = P(ZRegNumber%, SpecWinNumber%) + PofL
NEXT SpecWinNumber%
END IF
NEXT FacNumber%
NEXT ZRegNumber%

                                'the maximum spectral radiance within any
                                'spectral or spatial region is determined
                                'for display scaling
PMax = -99999
FOR ZRegNumber% = 1 TO NumZRegions%
    FOR SpecWinNumber% = 1 TO NumSpecWindows%
        IF (P(ZRegNumber%, SpecWinNumber%) > PMax) THEN PMax = P(ZRegNumber%,
                                                                    SpecWinNumber%)
    NEXT SpecWinNumber%
NEXT ZRegNumber%

                                'the spectral radiance is displayed for
                                'each spatial region
FOR ZRegNumber% = 1 TO NumZRegions%
    PSET ((ZSPatMin + (ZRegNumber% - 1) * ZSpatialSize + (1 / NumSpecWindows%) *
                                                ZSpatialSize) * Scale, WindowY1 + (P(ZRegNumber%, 1) /
                                                PMax) * (WindowY2 - WindowY1) / 4), 15
    FOR SpecWinNumber% = 2 TO NumSpecWindows%
        LINE -(ZSPatMin + (ZRegNumber% - 1) * ZSpatialSize + (SpecWinNumber% /
                                                NumSpecWindows%) * ZSpatialSize) * Scale, WindowY1 +
                                                (P(ZRegNumber%, SpecWinNumber%) / PMax) * (WindowY2 -
                                                WindowY1) / 4), 15
    NEXT SpecWinNumber%
NEXT ZRegNumber%

                                'wait for operator's response
LOCATE 28, 1
PRINT "Press any key to continue..."
DO
    LOOP WHILE INKEY$ = ""
LOCATE 28, 1
PRINT "

                                'the radiant flux for the total spectral
                                'region under consideration is determined
                                'for each spatial region and the entire
                                'penetrator
PTotal = 0
FOR ZRegNumber% = 1 TO NumZRegions%
    PRegion(ZRegNumber%) = 0
    FOR SpecWinNumber% = 1 TO NumSpecWindows%
        PTotal = PTotal + P(ZRegNumber%, SpecWinNumber%)
    
```

```

PRegion(ZRegNumber%) = PRegion(ZRegNumber%) + P(ZRegNumber%, SpecWinNumber%)
NEXT SpecWinNumber%
NEXT ZRegNumber%

```

'radiant flux integrated over the spatial
'regions is displayed for integrations
'beginning at the left and the right of
'the penetrator

```

PAccum = 0
FOR ZRegNumber% = 1 TO NumZRegions%
  PAccum = PAccum + PRegion(ZRegNumber%)
  CIRCLE ((ZSPatMin + (ZRegNumber% - .5) * ZSPatSize) * Scale, (PAccum / PTot) *
    (WindowY2 - WindowY1) + WindowY1), (WindowY2 - WindowY1) / 150, 15
  PAINT ((ZSPatMin + (ZRegNumber% - .5) * ZSPatSize) * Scale, (PAccum / PTot) *
    (WindowY2 - WindowY1) + WindowY1), 1, 15
  CIRCLE ((ZSPatMin + (ZRegNumber% - .5) * ZSPatSize) * Scale, ((PTot - PAccum) /
    PTot) * (WindowY2 - WindowY1) + WindowY1), (WindowY2 - WindowY1) /
    150, 15
  PAINT ((ZSPatMin + (ZRegNumber% - .5) * ZSPatSize) * Scale, ((PTot - PAccum) /
    PTot) * (WindowY2 - WindowY1) + WindowY1), 14, 15
NEXT ZRegNumber%

```

'the calculated radiant flux values are
'output to a data file

```
CALL OutputData
```

'wait for operator's response

```
DO
  LOOP WHILE INKEY$ = ""
```

```
SUB DeterPFacet (FacNumber%, SpecWinNumber%, PofL)
```

```
*****
THIS SUBROUTINE CALCULATES THE SPECTRAL RADIANT FLUX EMITTED BY A SINGLE
FACET AND COLLECTED BY THE DETECTOR
*****
```

'This subroutine calculates the spectral radiant flux (P of Lambda)
'from a single facet to the detector. P is the rate at which radiant
'energy is transferred from the facet to the detector. This quantity
'is determined by first calculating the spectral radiant emittance
'(W of Lambda) which is the radiant flux emitted per unit source area
'per unit wavelength interval at a particular wavelength and is
'calculated for a particular wavelength using the expression

$$W(L) = n \cdot \frac{C_1}{L^5} \cdot \frac{1}{\exp(C_2/LT) - 1}$$

'where: W(L) is the spectral radiant emittance in units of
watts/(m²*micron)
' n is the emissivity
' L represents lambda which is the wavelength in microns
' T is the absolute temperature in degrees Kelvin; K=C+273.16
' C1 is the first radiation constant equal to
3.7415E+8 Watt*micron⁴/m²
' C2 is the second radiation constant equal to
1.43879E+4 micron*degree K

'Making the assumption that the facet is a perfectly diffuse, or
'Lambertian, source, the spectral radiance (N of Lambda), which is
'the radiant flux per unit solid angle per unit area of source per
'unit wavelength interval at a particular wavelength (phew!), is
'calculated from the spectral radiant emittance through the simple
'relationship (N of Lambda)=(W of Lambda)/(Pi). Finally, the spectral
'radiant flux is calculated by multiplying the spectral radiant
'emittance by the effective source area, the solid angle subtended by

'the detector, and the span of the wavelength interval under
'consideration. The detector is assumed to have an effective area of
'1 square centimeter.

SHARED Area(), Temp(), Emis(), NormalCos(), SpecMin, SpecWindowSize
SHARED ProjRange, X(), Y(), Z()

'define the values of the radiation
'constants

C1 = 3.7415E+08 ' W*u^4/m^2
C2 = 14387.9 ' u*K

'calculate the value of the wavelength
'under consideration

Lambda = SpecMin + (SpecWinNumber% - 1) * SpecWindowSize

'calculate the spectral radiant emittance

FirstTerm = C1 / (Lambda ^ 5)

Exponent = C2 / (Lambda * (273.16 + Temp(FacNumber%)))

IF (Exponent < 60) THEN

SecondTerm = 1 / (EXP(Exponent) - 1)

ELSE

SecondTerm = 0

END IF

WofL = Emis(FacNumber%) * FirstTerm * SecondTerm

'calculate the spectral radiance

NofL = WofL / 3.14159

'calculate the effective source area

EffArea = Area(FacNumber%) * NormalCos(FacNumber%)

'calculate the average distance of the
'facet from the detector

Distance = 0

FOR Corner% = 1 TO 4

Distance = Distance + SQR((X(FacNumber%, Corner%) + ProjRange) ^ 2 +
Y(FacNumber%, Corner%) ^ 2 + Z(FacNumber%, Corner%) ^ 2) / 4

NEXT Corner%

'calculate the solid angle subtended by a
'1 square centimeter detector

SolidAngle = .0001 / Distance ^ 2

'calculate the spectral radiant flux
'incident on the 1 square centimeter
'detector

PofL = NofL * EffArea * SolidAngle * SpecWindowSize

END SUB

SUB DeterPlotColor (Temp, C)

'THIS SUBROUTINE ASSIGNS A GRAPHIC DISPLAY COLOR BASED ON THE TEMPERATURE
'OF A FACET

SHARED TempMin, TempMax

C = CINT(((Temp - TempMin) / (TempMax - TempMin)) * 13 + 1)

END SUB

SUB Init3DDisp

'THIS SUBROUTINE INITIALIZES AND SCALES THE GRAPHIC DISPLAY WINDOW, DEFINES
'THE GRAPHIC PALLETE, AND VISUALLY DISPLAYS THE SPATIAL EXTENT OF THE
'INDIVIDUAL IR CALCULATION REGIONS

SHARED WindowX1, WindowY1, WindowX2, WindowY2, NumZRegions%, ZSPatMin
SHARED ZSPatMax, ZSPatSize, Scale

DIM C%(15)

'graphic display is initialized and sized

SCREEN 12

VIEW (1, 1)-(638, 398)

WINDOW (WindowX1, WindowY1)-(WindowX2, WindowY2)

'graphic palette is defined

C%(0) = 65536 * 0 + 256 * 0 + 0

C%(14) = 65536 * 0 + 256 * 0 + 63

C%(13) = 65536 * 0 + 256 * 19 + 63

C%(12) = 65536 * 0 + 256 * 30 + 63

C%(11) = 65536 * 0 + 256 * 40 + 63

C%(10) = 65536 * 0 + 256 * 50 + 63

C%(9) = 65536 * 0 + 256 * 60 + 63

C%(8) = 65536 * 0 + 256 * 63 + 42

C%(7) = 65536 * 0 + 256 * 62 + 21

C%(6) = 65536 * 0 + 256 * 55 + 0

C%(5) = 65536 * 12 + 256 * 43 + 0

C%(4) = 65536 * 23 + 256 * 36 + 0

C%(3) = 65536 * 37 + 256 * 28 + 0

C%(2) = 65536 * 49 + 256 * 21 + 0

C%(1) = 65536 * 63 + 256 * 0 + 0

C%(15) = 65536 * 63 + 256 * 63 + 63

PALETTE USING C%(0)

'spatial extent of IR calculation regions
'is displayed graphically

FOR I% = 1 TO NumZRegions%

C% = 15

LINE ((ZSPatMin + (I% - 1) * ZSPatSize) * Scale, WindowY1)-((ZSPatMin + I% *
ZSPatSize) * Scale, WindowY2), C%, B

NEXT I%

END SUB

SUB OutputData

'THIS SUBROUTINE OUTPUTS THE TOTAL RADIANT FLUX, THE RADIANT FLUX FROM EACH
'SPATIAL REGION AND THE SPECTRAL RADIANT FLUX FROM EACH REGION TO A DATAFILE

SHARED File2\$, File1\$, PTotal, NumZRegions%, PRegion(), NumSpecWindows%
SHARED P()

OPEN File2\$ FOR OUTPUT AS #2

PRINT #2, "Input data file:"

PRINT #2, File1\$

PRINT #2, " "

PRINT #2, "Total radiant flux:"

PRINT #2, PTotal

PRINT #2, " "

FOR I% = 1 TO NumZRegions%

PRINT #2, " Spatial region #"; I%

PRINT #2, " Region radiant flux"

PRINT #2, " "; PRegion(I%)

FOR J% = 1 TO NumSpecWindows%

PRINT #2, " Spectral window #"; J%

```

        PRINT #2, "      "; P(I%, J%)
    NEXT J%
NEXT I%

```

```

CLOSE #2

```

```

END SUB

```

```

SUB Plot3DLine (X, Y, Z, C1)

```

```

*****
THIS SUBROUTINE PLOTS A DESIGNATED LINE ON THE GRAPHIC SCREEN IN A USER
SELECTED COLOR
*****

```

```

'Note that the horizontal direction
'corresponds to the Z axis and the
'vertical direction corresponds to
'the Y axis.

```

```

    SHARED Scale

```

```

    LINE -(Z * Scale, Y * Scale), C1

```

```

END SUB

```

```

SUB Plot3DPoint (X, Y, Z, C1)

```

```

*****
THIS SUBROUTINE PLOTS A DESIGNATED POINT ON THE GRAPHIC SCREEN IN A USER
SELECTED COLOR
*****

```

```

'Note that the horizontal direction
'corresponds to the Z axis and the
'vertical direction corresponds to
'the Y axis.

```

```

    SHARED Scale

```

```

    PSET (Z * Scale, Y * Scale), C1

```

```

END SUB

```

```

SUB ReadInputData1

```

```

*****
THIS SUBROUTINE MAKES THE FIRST PASS THROUGH A PREVIOUSLY GENERATED DATA
FILE THAT CONTAINS INFORMATION ABOUT A PENETRATOR'S GEOMETRY AND THERMAL
PROPERTIES. DURING THIS FIRST PASS THE LEADER PARAMETERS ARE INPUT AND THE
NUMBER OF SUBSEQUENT LINES OF FACET DATA IS DETERMINED
*****

```

```

    SHARED LengthNoseCone, DeltaZNoseCone, NumNoseConeLongSeg%, RadNoseCone
    SHARED NumNoseConeRadSeg%, LengthBody, DeltaZBody, NumBodyLongSeg%
    SHARED RadBody, NumBodyRadSeg%, NumFins%, ThickFin, LengthBaseFin
    SHARED LengthLeadEdgeFin, DeltaZFin, NumLeadEdgeLongSeg%
    SHARED NumNonLeadEdgeLongSeg%, HeightFin, DeltaRadFin, NumFinRadSeg%
    SHARED NumAftBodyRadSegPerFin%, Euler(), File1$, Scale, WindowX1
    SHARED WindowY1, WindowX2, WindowY2, NumFacets%

```

```

'previously generated datafile is opened

```

INPUT "Enter input data file name: "; File1\$

OPEN File1\$ FOR INPUT AS #1

'leader parameters that were used to
'generate the datafile are input and
'displayed on the screen

INPUT #1, leader\$
INPUT #1, LengthNoseCone
PRINT leader\$; LengthNoseCone

INPUT #1, leader\$
INPUT #1, DeltaZNoseCone
PRINT leader\$; DeltaZNoseCone

INPUT #1, leader\$
INPUT #1, NumNoseConeLongSeg%
PRINT leader\$; NumNoseConeLongSeg%

INPUT #1, leader\$
INPUT #1, RadNoseCone
PRINT leader\$; RadNoseCone

INPUT #1, leader\$
INPUT #1, NumNoseConeRadSeg%
PRINT leader\$; NumNoseConeRadSeg%

INPUT #1, leader\$
INPUT #1, LengthBody
PRINT leader\$; LengthBody

INPUT #1, leader\$
INPUT #1, DeltaZBody
PRINT leader\$; DeltaZBody

INPUT #1, leader\$
INPUT #1, NumBodyLongSeg%
PRINT leader\$; NumBodyLongSeg%

INPUT #1, leader\$
INPUT #1, RadBody
PRINT leader\$; RadBody

INPUT #1, leader\$
INPUT #1, NumBodyRadSeg%
PRINT leader\$; NumBodyRadSeg%

INPUT #1, leader\$
INPUT #1, NumFins%
PRINT leader\$; NumFins%

INPUT #1, leader\$
INPUT #1, ThickFin
PRINT leader\$; ThickFin

INPUT #1, leader\$
INPUT #1, LengthBaseFin
PRINT leader\$; LengthBaseFin

INPUT #1, leader\$
INPUT #1, LengthLeadEdgeFin
PRINT leader\$; LengthLeadEdgeFin

INPUT #1, leader\$
INPUT #1, DeltaZFin
PRINT leader\$; DeltaZFin


```

INPUT #1, leader$
INPUT #1, NumLeadEdgeLongSeg%
PRINT leader$; NumLeadEdgeLongSeg%

INPUT #1, leader$
INPUT #1, NumNonLeadEdgeLongSeg%
PRINT leader$; NumNonLeadEdgeLongSeg%

INPUT #1, leader$
INPUT #1, HeightFin
PRINT leader$; HeightFin

INPUT #1, leader$
INPUT #1, DeltaRadFin
PRINT leader$; DeltaRadFin

INPUT #1, leader$
INPUT #1, NumFinRadSeg%
PRINT leader$; NumFinRadSeg%

INPUT #1, leader$
INPUT #1, NumAftBodyRadSegPerFin%
PRINT leader$; NumAftBodyRadSegPerFin%

INPUT #1, leader$
INPUT #1, Euler(1)
PRINT leader$; Euler(1)

INPUT #1, leader$
INPUT #1, Euler(2)
PRINT leader$; Euler(2)

INPUT #1, leader$
INPUT #1, Euler(3)
PRINT leader$; Euler(3)

INPUT #1, leader$
INPUT #1, NoseForwTemp
PRINT leader$; NoseForwTemp

INPUT #1, leader$
INPUT #1, NoseRearTemp
PRINT leader$; NoseRearTemp

INPUT #1, leader$
INPUT #1, NoseEmis
PRINT leader$; NoseEmis

INPUT #1, leader$
INPUT #1, BodyForwTemp
PRINT leader$; BodyForwTemp

INPUT #1, leader$
INPUT #1, BodyRearTemp
PRINT leader$; BodyRearTemp

INPUT #1, leader$
INPUT #1, BodyEmis
PRINT leader$; BodyEmis

INPUT #1, leader$
INPUT #1, FinOuterWRTInnerTemp
PRINT leader$; FinOuterWRTInnerTemp

INPUT #1, leader$
INPUT #1, FinLeadTemp

```

```

PRINT leader$; FinLeadTemp

INPUT #1, leader$
INPUT #1, FinTrailTemp
PRINT leader$; FinTrailTemp

INPUT #1, leader$
INPUT #1, FinEmis
PRINT leader$; FinEmis

INPUT #1, leader$
INPUT #1, AftBodyForwTemp
PRINT leader$; AftBodyForwTemp

INPUT #1, leader$
INPUT #1, AftBodyRearTemp
PRINT leader$; AftBodyRearTemp

INPUT #1, leader$
INPUT #1, AftBodyEmis
PRINT leader$; AftBodyEmis

INPUT #1, leader$
INPUT #1, File1$
PRINT leader$; File1$

INPUT #1, leader$
INPUT #1, Scale
PRINT leader$; Scale

INPUT #1, leader$
INPUT #1, WindowX1
PRINT leader$; WindowX1

INPUT #1, leader$
INPUT #1, WindowY1
PRINT leader$; WindowY1

INPUT #1, leader$
INPUT #1, WindowX2
PRINT leader$; WindowX2

INPUT #1, leader$
INPUT #1, WindowY2
PRINT leader$; WindowY2
PRINT

                                'number of lines of data that describes
                                'each facet is determined

NumFacets% = 0
DO
    INPUT #1, Test$
    NumFacets% = NumFacets% + 1
    LOOP WHILE Test$ <> "END"
NumFacets% = (NumFacets% - 1) / 2

                                'datafile is closed

CLOSE #1

END SUB

SUB ReadInputData2
*****

'THIS SUBROUTINE MAKES THE SECOND PASS THROUGH THE PREVIOUSLY GENERATED
DATA
'FILE THAT DESCRIBES THE PENETRATOR GEOMETRY AND THERMAL PROPERTIES. DURING

```

'THIS PASS THE LEADER INFORMATION IS IGNORED BUT THE SUBSEQUENT LINES THAT
'DEFINE THE INDIVIDUAL FACET PARAMETERS ARE INPUT

SHARED File1\$, NumFacets%, Type\$(), X(), Y(), Z(), NormalCos()
SHARED Area(), Temp(), Emis()

'datafile is reopened

OPEN File1\$ FOR INPUT AS #1

'leader data is input but not used

INPUT #1, leader\$
INPUT #1, LengthNoseCone

INPUT #1, leader\$
INPUT #1, DeltaZNoseCone

INPUT #1, leader\$
INPUT #1, NumNoseConeLongSeg%

INPUT #1, leader\$
INPUT #1, RadNoseCone

INPUT #1, leader\$
INPUT #1, NumNoseConeRadSeg%

INPUT #1, leader\$
INPUT #1, LengthBody

INPUT #1, leader\$
INPUT #1, DeltaZBody

INPUT #1, leader\$
INPUT #1, NumBodyLongSeg%

INPUT #1, leader\$
INPUT #1, RadBody

INPUT #1, leader\$
INPUT #1, NumBodyRadSeg%

INPUT #1, leader\$
INPUT #1, NumFins%

INPUT #1, leader\$
INPUT #1, ThickFin

INPUT #1, leader\$
INPUT #1, LengthBaseFin

INPUT #1, leader\$
INPUT #1, LengthLeadEdgeFin

INPUT #1, leader\$
INPUT #1, DeltaZFin

INPUT #1, leader\$
INPUT #1, NumLeadEdgeLongSeg%

INPUT #1, leader\$
INPUT #1, NumNonLeadEdgeLongSeg%

INPUT #1, leader\$
INPUT #1, HeightFin

INPUT #1, leader\$
INPUT #1, DeltaRadFin

INPUT #1, leader\$
INPUT #1, NumFinRadSeg%

INPUT #1, leader\$
INPUT #1, NumAftBodyRadSegPerFin%

INPUT #1, leader\$
INPUT #1, Euler

INPUT #1, leader\$
INPUT #1, Euler

INPUT #1, leader\$
INPUT #1, Euler

INPUT #1, leader\$
INPUT #1, NoseForwTemp

INPUT #1, leader\$
INPUT #1, NoseRearTemp

INPUT #1, leader\$
INPUT #1, NoseEmis

INPUT #1, leader\$
INPUT #1, BodyForwTemp

INPUT #1, leader\$
INPUT #1, BodyRearTemp

INPUT #1, leader\$
INPUT #1, BodyEmis

INPUT #1, leader\$
INPUT #1, FinOuterWRTInnerTemp

INPUT #1, leader\$
INPUT #1, FinLeadTemp

INPUT #1, leader\$
INPUT #1, FinTrailTemp

INPUT #1, leader\$
INPUT #1, FinEmis

INPUT #1, leader\$
INPUT #1, AftBodyForwTemp

INPUT #1, leader\$
INPUT #1, AftBodyRearTemp

INPUT #1, leader\$
INPUT #1, AftBodyEmis

INPUT #1, leader\$
INPUT #1, File1\$

INPUT #1, leader\$
INPUT #1, Scale

INPUT #1, leader\$
INPUT #1, WindowX1

INPUT #1, leader\$
INPUT #1, WindowY1

```

INPUT #1, leader$
INPUT #1, WindowX2

INPUT #1, leader$
INPUT #1, WindowY2

                                'data about the geometry and thermal
                                'properties of each facet is input
FOR I% = 1 TO NumFacets%
  INPUT #1, Type$(I%), X(I%, 1), Y(I%, 1), Z(I%, 1), X(I%, 2), Y(I%, 2), Z(I%, 2), X(I%, 3),
  Y(I%, 3), Z(I%, 3), X(I%, 4), Y(I%, 4), Z(I%, 4),
  NormalCos(I%), Area(I%), Temp(I%), Emis(I%)

  NEXT I%

                                'datafile is closed
CLOSE #1
END SUB

```

INTENTIONALLY LEFT BLANK.

<u>NO. OF COPIES</u>	<u>ORGANIZATION</u>
2	DEFENSE TECHNICAL INFO CTR ATTN DTIC DDA 8725 JOHN J KINGMAN RD STE 0944 FT BELVOIR VA 22060-6218
1	DIRECTOR US ARMY RESEARCH LAB ATTN AMSRL OP SD TA 2800 POWDER MILL RD ADELPHI MD 20783-1145
3	DIRECTOR US ARMY RESEARCH LAB ATTN AMSRL OP SD TL 2800 POWDER MILL RD ADELPHI MD 20783-1145
1	DIRECTOR US ARMY RESEARCH LAB ATTN AMSRL OP SD TP 2800 POWDER MILL RD ADELPHI MD 20783-1145
	<u>ABERDEEN PROVING GROUND</u>
2	DIR USARL ATTN AMSRL OP AP L (305)

NO. OF
COPIES ORGANIZATION

5 DIRECTOR
US ARMY RESEARCH LAB
ATTN AMSRL PS
V GELNOVATCH
R HAMLEN
J KEY
AMSRL PS D M TOMPSETT
AMSRL PS T R REITMEYER
BLDG 2700
FT MONMOUTH NJ 07703-5601

1 DIRECTOR
US ARMY RESEARCH LAB
ATTN AMSRL SL E
G MARES
WSMR NM 88002-5501

2 VHCLE STRCTRS DIRECTORATE
ATTN AMSRL VS L D HOD
AMSRL VS S F BARTLETT
MS 266
NASA LANGLEY RSRCH CTR
HAMPTON VA 23681-0001

2 VHCLE PRPLSN DIRECTORATE
ATTN AMSRL VP C R BILL
AMSRL VP T G BOBULA
21000 BROOKPARK RD
CLEVELAND OH 44135-3191

NO. OF
COPIES ORGANIZATION

ABERDEEN PROVING GROUND

25 DIR, USARL
ATTN: AMSRL-MA, J. DIGNAM (CNR)
AMSRL-MA-A, D. VIECHNICKI (CNR)
AMSRL-SE, J. MILLER (ALC)
AMSRL-SE-E, J. PELLEGRINO (ALC)
AMSRL-WT-N, J. INGRAM (ALC)
AMSRL-SL-B, P. DEITZ
AMSRL-SL-C, W. HUGHES
AMSRL-WT-P, A. HORST
AMSRL-WT-T, W. MORRISON
AMSRL-WT-W, C. MURPHY, JR.
AMSRL-WT-WD,
A. NIILER
P. BERNING
R. BOSSOLI
S. CORNELISON
A. GAUSS, JR.
C. HOLLANDSWORTH
C. HUMMER
L. KECSKES
T. KOTTKE
M. MCNEIR
J. POWELL
A. PRAKASH
D. STRENCWILK
C. STUMPFEL
G. THOMSON

USER EVALUATION SHEET/CHANGE OF ADDRESS

This Laboratory undertakes a continuing effort to improve the quality of the reports it publishes. Your comments/answers to the items/questions below will aid us in our efforts.

1. ARL Report Number/Author ARL-MR-329 (Kottke) Date of Report August 1996

2. Date Report Received _____

3. Does this report satisfy a need? (Comment on purpose, related project, or other area of interest for which the report will be used.) _____

4. Specifically, how is the report being used? (Information source, design data, procedure, source of ideas, etc.) _____

5. Has the information in this report led to any quantitative savings as far as man-hours or dollars saved, operating costs avoided, or efficiencies achieved, etc? If so, please elaborate. _____

6. General Comments. What do you think should be changed to improve future reports? (Indicate changes to organization, technical content, format, etc.) _____

CURRENT
ADDRESS

Organization

Name

Street or P.O. Box No.

City, State, Zip Code

7. If indicating a Change of Address or Address Correction, please provide the Current or Correct address above and the Old or Incorrect address below.

OLD
ADDRESS

Organization

Name

Street or P.O. Box No.

City, State, Zip Code

(Remove this sheet, fold as indicated, tape closed, and mail.)
(DO NOT STAPLE)

DEPARTMENT OF THE ARMY

OFFICIAL BUSINESS

BUSINESS REPLY MAIL

FIRST CLASS PERMIT NO 0001,APG,MD

POSTAGE WILL BE PAID BY ADDRESSEE

DIRECTOR
US ARMY RESEARCH LABORATORY
ATTN AMSRL WT WD
ABERDEEN PROVING GROUND MD 21005-5066



NO POSTAGE
NECESSARY
IF MAILED
IN THE
UNITED STATES

